

An optimization approach for well-targeted transcranial direct current stimulation

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Abstract

Transcranial direct current stimulation is a non-invasive brain stimulation technique which modifies neural excitability by providing weak currents through scalp electrodes. The aim of this study is to introduce and analyze a novel optimization method for safe and well-targeted multi-array tDCS. For optimization, we consider an optimal control problem for a Laplace equation with Neumann boundary conditions with control and point-wise gradient state constraints. We prove existence and residual and objective convergence results for the proposed methods and provide computer simulation results in a highly realistic six-compartment geometry-adapted hexahedral head model. For discretization of the proposed minimization problem the finite element method is employed and the existence of at least one minimizer to the discretized optimization problem is shown. For numerical solution of the corresponding discretized problem we employ the alternating direction method of multipliers and comprehensively examine the cortical current flow field with regard to focality, target intensity and orientation. The numerical results reveal that the optimized current flow fields show significantly higher focality and, in most cases, higher directional agreement to the target vector in comparison to standard bipolar electrode montages.

1 Introduction

Transcranial direct current stimulation (tDCS) is a non-invasive, inexpensive and easy-to-perform brain stimulation technique which modifies neural excitability [19]. Changes in neural membrane potentials are induced in a polarity-dependent manner, for example, in a motor cortex study, anodal stimulation right over the motor cortex enhances cortical excitability, whereas cathodal stimulation inhibits it [19]. Recently, tDCS has been applied successfully in the treatment of neurological and neuropsychiatric disorders such as epilepsy [11], depression [4] and Alzheimer disease [10]. The effects of tDCS can be preserved for more than one hour after stimulation [20].

The conventional strategy is to apply the current density $\sigma \nabla \Phi$ via two large electrodes, with the active electrode (anode) to be placed above the presumed target region and the reference electrode (cathode) far away from the target region [19, 20]. Accurate and detailed finite element (FE) head models have been created to investigate the induced current density distribution [25, 8, 23]. While significant effects of stimulation as compared to sham were reported [4, 11, 19], computer simulation studies have revealed that

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the induced cortical current flow fields are very widespread with often strongest current density amplitudes in non-target brain regions [25, 23]. It is therefore a matter of debate whether the effects of stimulation are driven by the target brain region or elicited by adjacent cortical lobes [23].

In order to overcome the limitations of conventional bipolar electrode montages, algorithmic-based sensor optimization approaches were presented [8, 23, 17]. While Im and colleagues [17] searched for two electrode locations which generate maximal current flow towards a certain target direction, Dmochowski and colleagues [8] used a multi-channel array consisting of 64 fixed electrode locations to calculate optimized stimulation protocols for presumed target regions. They employed radial and tangential targets and reported that compared with conventional electrode montages their optimization approach achieved electric fields which exhibit simultaneously greater focality and target intensity at cortical targets using the same total current applied. While the optimization results are very promising and a pilot study using multi-array tDCS devices for rehabilitation after stroke has been conducted [9], to our knowledge, there is currently no study providing an in-depth analysis of mathematical models for multi-array tDCS optimization.

Given a volume conductor model Ω with a fixed electrode arrangement and a target vector \mathbf{e} in Ω_t with $\Omega_t \subset \Omega$ being the target cortical area, the optimization approach estimates an optimal applied current pattern at the fixed electrodes. A Laplace equation with inhomogeneous Neumann boundary conditions is used to calculate the induced current density distribution [25] which is to be controlled by the boundary condition to ensure safe and focused stimulation. Therefore, the optimization problem for tDCS is in the class of control problems with Neumann boundary conditions [18].

This paper is organized as follows: In Section 2 we establish the mathematical model of tDCS and introduce the optimization problem for multi-channel tDCS. In Section 3 we show existence of at least one minimizer to the optimization problem and the FE method is used for numerical discretization. In Section 4 we derive the algorithm for sensor optimization. Section 5 provides optimization results in a highly-realistic six-compartment head model (skin, skull compacta, skull spongiosa, CSF, gray and white matter) with white matter anisotropy. Furthermore, a conclusion and outlook section is presented. Finally, in the Appendix, we prove residual and objective convergence results for the proposed optimization method.

2 Mathematical Model of tDCS

In order to calculate the current flow field induced by tDCS, the quasistatic approximation to Maxwell's equations is applied [25]. This yields the *tDCS forward problem*

$$\begin{aligned} \nabla \cdot \sigma \nabla \Phi &= 0 & \text{in } \Omega \\ \langle \sigma \nabla \Phi, \mathbf{n} \rangle &= \mathbf{I} & \text{on } \Gamma \\ \Phi &= 0 & \text{on } \Gamma_D \end{aligned}$$

with Φ being the electric potential, $\sigma \in (L^\infty)^{3 \times 3}$ being an anisotropic conductivity tensor, \mathbf{I} being the applied current pattern at the electrodes with non-zero values only at the electrode surfaces, \mathbf{n} being the outward normal vector and Γ being the boundary of the domain Ω . Furthermore, a Dirichlet boundary condition on Γ_D is used to ensure that a solution to the tDCS forward problem is unique. We introduce the Sobolev space

$$H_\diamond^{-\frac{1}{2}}(\Gamma) := \{u \in H^{-\frac{1}{2}}(\Gamma) \mid \int_\Gamma u(s) \, ds = 0\} \subset H^{-\frac{1}{2}}(\Gamma)$$

with $H^{-\frac{1}{2}}(\Gamma)$ being the standard Sobolev space related to Neumann traces of H^1 -functions on Γ . The integral in the above definition has to be interpreted as a duality product with the constant function equal to one, which is in $H^{\frac{1}{2}}(\Gamma)$.

Under standard and naturally satisfied regularity assumptions, there exists a unique solution $\Phi \in H^1(\Omega)$ to the tDCS forward problem, which can be shown by the Lax-Milgram Lemma:

Theorem 1. *Let $\sigma \in (L^\infty)^{3 \times 3}$ with $\sigma \geq \sigma_0 I_{3 \times 3}$ and let $\mathbf{I} \in H_\diamond^{-\frac{1}{2}}(\Gamma)$. Then there exists a solution $\Phi \in H^1(\Omega)$ to the tDCS forward problem. The solution is unique if Γ_D has positive measure and the following norm estimate holds:*

$$\|\Phi\|_{H^1} \leq C \|\mathbf{I}\|_{H^{-\frac{1}{2}}}$$

For current density optimization, a multi-channel array consisting of 74 fixed electrode locations (the locations of an extended 10-10 EEG electrode system) is used and optimized applied current patterns are calculated for presumed targets. Figure 1 illustrates an overview of the optimization setup in a two-dimensional model. Optimally, the induced current density distribution is maximal in the target region Ω_t and zero in non-target regions $\Omega_r = \Omega \setminus \Omega_t$. Physically, a focal stimulation without stimulating non-target regions is not possible as the current has to flow through the volume to reach the target region. Therefore, the current density is restricted by $\epsilon > 0$ such that

$$|\sigma \nabla \Phi| \leq \epsilon \quad \text{in } \Omega_r.$$

Secondly, the total current applied to all electrodes is limited to 2 mA, a commonly used safety criterium [8].

For effective stimulation, the optimized current density distribution should be oriented perpendicularly to the cortical surface [3, 6]. Also, the direction is important as shown by Bindman and colleagues [3] and Creutzfeldt and colleagues [6] who were able to demonstrate in physical measurements in rats and cats, respectively, that the neural firing rate is strongly influenced by the direction of the field to the cortical surface. Perpendicularly-inwards (and parallel to the long apical dendrites of the large pyramidal cells in cortical layer V) stimulation, i.e. anodal stimulation, strongly enhanced the activity of the cortical neurons, whereas radially-outwards stimulation, i.e. cathodal stimulation, inhibited it. We thus maximize $\int_{\Omega_t} \langle \sigma \nabla \Phi, \mathbf{e} \rangle d\mathbf{x}$ with $\mathbf{e} \subset \Omega_t$ being a vector parallel and radially-inwards-oriented to the cortical surface [3, 6].

In the following we reformulate the current density constraint in the whole domain as $\omega |\sigma \nabla \Phi| \leq \epsilon$ with a weight $\omega = 1$ in Ω_r and $0 < \omega \ll 1$ in Ω_t . Thus, we consider the constrained optimization problem

$$\begin{aligned} \text{(P)} \quad & - \int_{\Omega_t} \langle \sigma \nabla \Phi, \mathbf{e} \rangle d\mathbf{x} \rightarrow \min_{\mathbf{I} \in H_\diamond^{-\frac{1}{2}}(\Gamma)} \\ & \text{subject to} \quad \omega |\sigma \nabla \Phi| \leq \epsilon \\ & \int_{\Gamma} |\mathbf{I}| d\mathbf{x} \leq 4 \\ & \nabla \cdot \sigma \nabla \Phi = 0 \quad \text{in } \Omega \\ & \langle \sigma \nabla \Phi, \mathbf{n} \rangle = \mathbf{I} \quad \text{on } \partial\Gamma \\ & \Phi = 0 \quad \text{on } \Gamma_D \end{aligned}$$

which is a control problem with Neumann boundary conditions [18]. Note that safety limitation on the inflow current is a *control constraint*, while the limit on the current

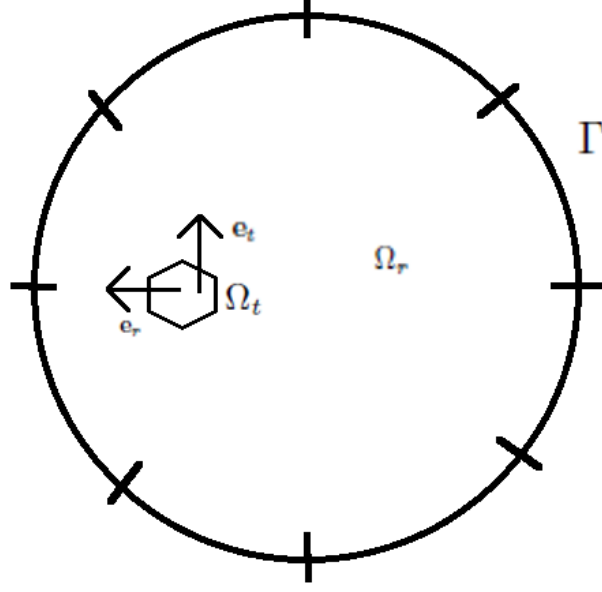


Figure 1: Optimization setup in a two-dimensional model. The target region Ω_t , a radial (\mathbf{e}_r) and tangential (\mathbf{e}_t) target vector and the boundary Γ of the volume conductor model Ω are demonstrated. The electrodes are depicted with solid lines.

density outside the target region is a *state constraint*. Also, the state constraint with $\omega > 0$ ensures that $\nabla\Phi$ is bounded in $L^\infty(\Omega)$ and due to the embedding theorem also bounded in $L^2(\Omega)$. This implies that $\Phi \in H^1(\Omega)$ and due to the trace theorem $\Phi|_\Gamma \in H^{\frac{1}{2}}(\Gamma)$. Since $\sigma \in (L^\infty)^{3 \times 3}$ this implies that $\langle \sigma \nabla \Phi, \mathbf{n} \rangle$ is bounded in $H^{-\frac{1}{2}}(\Gamma)$.

Remark 1. *The constrained optimization problem (P) is a rather challenging optimal control problem. Firstly, the current density distribution $\sigma \nabla \Phi$ is optimized, while many other applications require to optimize the potential field Φ . Secondly, a point-wise gradient state constraint is used. While optimal control problems with state constraints were frequently used [14], not much attention was given to gradient state constraints only until recently [22]. Thirdly, we look for a control function \mathbf{I} vanishing on large parts of the boundary, known as sparsity optimal control problem [16]. Indeed, we rather look for \mathbf{I} as a combination of concentrated measures rather than an L^1 -function, so the above integral formulation has to be understood as formal notation for the total variation of the Radon measure identified with \mathbf{I} . This will be made precise in the next section.*

Applying Gauss' Theorem to $\int_{\Omega_t} \langle \sigma \nabla \Phi, \mathbf{e} \rangle d\mathbf{x}$ provides a further motivation for the proposed objective functional. Assuming σ and \mathbf{e} locally constant we have

$$\int_{\Omega_t} \langle \sigma \nabla \Phi, \mathbf{e} \rangle d\mathbf{x} = \int_{\Omega_t} \sigma \Phi \nabla \cdot \mathbf{e} + \mathbf{e} \nabla \sigma \Phi d\mathbf{x} = \int_{\Omega_t} \nabla \cdot (\sigma \Phi \mathbf{e}) d\mathbf{x} = \int_{\partial \Omega_t} \langle \sigma \Phi \mathbf{e}, \mathbf{n} \rangle d\sigma$$

In order to maximize the current densities along the target direction, the potential should be maximized where the target vector \mathbf{e} is oriented parallel to the outward normal vector \mathbf{n} on $\partial \Omega_t$ and minimized where it is antiparallel.

3 Optimal Control Problem

The goal of this section is to provide insight into the existence theory of at least one minimizer to the tDCS optimization problem (\mathbf{P}) . Furthermore, we show existence of at least one minimizer to a simplified optimization problem without control constraint at the electrodes. Finally, the finite element method is used for numerical discretization of the considered optimization procedure.

3.1 Continuous formulation

We now reconsider the optimization problem (\mathbf{P}) . In order to provide a rigorous formulation of the safety constraint we interpret \mathbf{I} as a Radon measure in the space $\mathcal{M}(\Gamma)$, whose norm, i.e. the total variation of a measure, is an appropriate replacement for the L^1 -norm. The constraint then becomes

$$\|\mathbf{I}\|_{\mathcal{M}(\Gamma)} \leq 4$$

In order to obtain a unified formulation also allowing for other design constraints respectively a discrete electrode setup, we introduce a feasible set $\mathcal{D}(\Gamma) \subset H_\diamond^{-\frac{1}{2}}(\Gamma)$. To further simplify notation we define an operator A via

$$A : H_\diamond^{-\frac{1}{2}}(\Gamma) \rightarrow L^2(\Omega)^3, \quad \mathbf{I} \mapsto \sigma \nabla \Phi.$$

Since $\mathbf{I} \in \mathcal{D}(\Gamma) \subset H_\diamond^{-\frac{1}{2}}(\Gamma)$, the boundary value problem for the Poisson equation has a unique solution $\Phi \in H^1(\Omega)$ bounded by a multiple of the norm of \mathbf{I} as guaranteed by Theorem 1. This implies that A is a well-defined linear operator. Hence we can substitute $\sigma \nabla \Phi = A\mathbf{I}$ in (\mathbf{P}) , which leads to the following equivalent reformulation

$$\begin{aligned} (\mathbf{P}_\epsilon^2) \quad & - \int_{\Omega_t} \langle A\mathbf{I}, \mathbf{e} \rangle d\mathbf{x} \rightarrow \min_{\mathbf{I} \in \mathcal{D}(\Gamma)} \\ & \text{subject to} \quad \omega |A\mathbf{I}| \leq \epsilon \\ & \|\mathbf{I}\|_{\mathcal{M}(\Gamma)} \leq 4. \end{aligned}$$

The existence of at least one minimizer $\mathbf{I} \in \mathcal{D}(\Gamma)$ to (\mathbf{P}_ϵ^2) is the topic of the following theorem.

Theorem 2. *Let $\mathcal{D}(\Gamma)$ be weakly closed in $H_\diamond^{-\frac{1}{2}}(\Gamma)$, let $0 \in \mathcal{D}(\Gamma)$ and let $\epsilon > 0$. Then there exists at least one minimizer $\mathbf{I} \in \mathcal{D}(\Gamma)$ of the convex optimization problem (\mathbf{P}_ϵ^2) .*

Proof. An easy computation reveals that $\mathbf{I} = 0 \in \mathcal{D}(\Gamma)$ is feasible for (\mathbf{P}_ϵ^2) , i.e. the set of feasible points is not empty. Moreover, it is closed in the weak-star topology of $H_\diamond^{-\frac{1}{2}}(\Gamma) \cap \mathcal{M}(\Gamma)$, which can be seen as follows: First of all the norm in $\mathcal{M}(\Gamma)$ is lower semicontinuous with respect to weak-star convergence in this space, which implies that a limit of feasible points satisfies the safety constraint as well. Moreover, weak convergence of a sequence \mathbf{I}^k in $H_\diamond^{-\frac{1}{2}}(\Gamma)$ implies weak convergence of $A\mathbf{I}^k$ in $L^2(\Omega)^3$, which implies that the limit satisfies the state constraint due to the weak closedness of pointwise constraints in L^2 . Moreover, the feasible set is obviously bounded in $\mathcal{M}(\Omega)$ due to the safety constraint and in $H_\diamond^{-\frac{1}{2}}(\Gamma)$ since any feasible \mathbf{I} is the Neumann trace of a function bounded in $W^{1,\infty}(\Omega)$ and thus in $H^1(\Omega)$. Hence, the Banach-Alaoglu Theorem implies compactness in the weak-star topology. Since the objective is a bounded linear functional and in particular weak-star lower semicontinuous we obtain the existence of a minimizer by standard reasoning. \square

We observe that the objective as well as all terms involved in the constraints of the optimal control problem are one-homogeneous. This allows us to renormalize the unknown and in this way eliminate the safety constraint. This motivates the following simplified version:

$$\begin{aligned}
(\mathbf{P}_\epsilon) \quad & - \int_{\Omega_t} \langle A\mathbf{I}, \mathbf{e} \rangle d\mathbf{x} \rightarrow \min_{\mathbf{I} \in \mathcal{D}(\Gamma)} \\
& \text{subject to} \quad \omega |A\mathbf{I}| \leq \epsilon
\end{aligned}$$

In the Appendix, we show objective and residual convergence results for the simplified optimization problem (\mathbf{P}_ϵ) .

By renormalizing a minimizer of (\mathbf{P}_ϵ) we can obtain a minimizer for the full optimization problem (\mathbf{P}_ϵ^2) with safety constraint for the control, which of course only holds if the total variation of the minimizer is finite:

Theorem 3. *Let $\epsilon > 0$ be a threshold parameter and $\mathbf{I} \in \mathcal{M}(\Gamma) \cap H_\diamond^{-\frac{1}{2}}(\Gamma)$ be a minimizer of the simplified minimization problem (\mathbf{P}_ϵ) . Then $\tilde{\mathbf{I}} = \frac{4\mathbf{I}}{\|\mathbf{I}\|_{\mathcal{M}(\Gamma)}}$ is a minimizer of (\mathbf{P}_δ^2) with $\delta = \frac{4\epsilon}{\|\mathbf{I}\|_{\mathcal{M}(\Gamma)}}$.*

Proof. An easy calculation reveals that $\tilde{\mathbf{I}} = \frac{4\mathbf{I}}{\|\mathbf{I}\|_{\mathcal{M}(\Gamma)}}$ fulfills the control and state constraint of (\mathbf{P}_δ^2) with $\delta = \frac{4\epsilon}{\|\mathbf{I}\|_{\mathcal{M}(\Gamma)}}$ \square

At a first glance the usefulness of Theorem 3 might appear limited, since the relation between the constraint bounds ϵ and δ is quite implicit, depending on the minimizer of the second problem. However, since there is no natural choice of the bound in either case one can choose δ or ϵ in appropriate ranges equally well. It turns out however that (\mathbf{P}_ϵ) is somewhat easier in particular with respect to numerical solutions. Moreover, it offers a better position to introduce sparsity constraints on the control by additional penalization, which is the subject of the following discussion.

3.2 Penalized Problem Formulation

In order to control the applied current pattern at the fixed electrodes, the minimization problem (\mathbf{P}_ϵ) is extended by two penalties. While an L_2 term $\alpha \int_\Gamma \mathbf{I}^2 d\mathbf{x}$ is introduced to penalize the energy of the applied current pattern, an L_1 penalty $\beta \|\mathbf{I}\|_{\mathcal{M}(\Gamma)}$ is used to minimize the number of active electrodes in the minimization procedure. The latter has to be reinterpreted in the same way as the safety constraint in terms of Radon measures. This leads to the following minimization problem

$$\begin{aligned}
(\mathbf{P}_\epsilon^{\alpha,\beta}) \quad & - \int_{\Omega_t} \langle A\mathbf{I}, \mathbf{e} \rangle d\mathbf{x} + \alpha \int_\Gamma \mathbf{I}^2 d\mathbf{x} + \beta \|\mathbf{I}\|_{\mathcal{M}(\Gamma)} \rightarrow \min_{\mathbf{I} \in \mathcal{D}(\Gamma)} \\
& \text{subject to} \quad \omega |A\mathbf{I}| \leq \epsilon
\end{aligned}$$

We call the minimization problem $(\mathbf{P}_\epsilon^{\alpha,\beta})$ with $\alpha > 0, \beta = 0$ and $\alpha = 0, \beta > 0$ to be the L_2 regularized optimization procedure (L2R) and the L_1 regularized optimization procedure (L1R), respectively. If both penalties are active, the penalty term is also known as elastic net.

Since the L^2 penalty adds strict convexity to the problem, we can obtain uniqueness of a minimizer together with existence via analogous arguments as above:

Theorem 4. *Let $\mathcal{D}(\Gamma)$ be weakly closed in $H_\diamond^{-\frac{1}{2}}$, $0 \in \mathcal{D}(\Gamma)$, and let $\alpha > 0$ and $\beta = 0$. Then there exists a unique minimizer $\mathbf{I} \in L^2(\Gamma)$ to the $L2R$ constrained optimization problem $(\mathbf{P}_\epsilon^{\alpha,0})$. In the latter statement, $\beta = 0$ can even be generalized to $\beta \geq 0$.*

For the problem with pure L^1 -penalization the proof of existence is almost identical to the one of Theorem 3 and we hence conclude:

Theorem 5. *Let \mathcal{D} be weakly closed in $H_\diamond^{-\frac{1}{2}}$ and let $\alpha = 0$ and $\beta > 0$. Then there exists at least one minimizer $\mathbf{I} \in \mathcal{M}(\Gamma) \cap \mathcal{D}(\Gamma)$ to the $L1R$ constrained optimization problem $(\mathbf{P}_\epsilon^{0,\beta})$.*

3.3 Discrete Problem

For numerical discretization of the considered optimization problem we use the finite element method. Let us discretize $\mathbf{I} = \sum_{i=1}^S I_i \phi_i$ with ϕ_i being finite element basis functions. From the fact that \mathbf{I} has mean zero we can eliminate I_S . Furthermore, we introduce mappings A_1 and A_2 incorporating the discretizations:

$$\begin{aligned} A_1 : \mathbb{R}^{S-1}(\Gamma) &\rightarrow \mathcal{D}(\Gamma), \quad \mathbf{I}_S = (I_i) \mapsto \mathbf{I} = \sum_{i=1}^S I_i \phi_i \\ A_2 : L^2(\Omega)^3 &\rightarrow \mathbb{R}^{3N}(\Omega), \quad \sigma \nabla \Phi \mapsto (\sigma \nabla \Phi)_i \end{aligned}$$

with N the number of elements and define the discretized operator $A_2 \circ A \circ A_1 = B \in \mathbb{R}^{3N \times (S-1)}$.

As the target vector \mathbf{e} is only defined in the target region, we define a continuous mapping $\tilde{\mathbf{e}} : \Omega_t \mapsto \mathbb{R}^{3N}(\Omega)$

$$\tilde{\mathbf{e}}_i = \begin{cases} \mathbf{e}_i, & \text{if } i \in \Omega_t \\ 0, & \text{otherwise} \end{cases}$$

and replace $\langle B\mathbf{I}_S, \mathbf{e} \rangle$ by $\langle B\mathbf{I}_S, \tilde{\mathbf{e}} \rangle$, since $\langle B\mathbf{I}_S, \tilde{\mathbf{e}} \rangle = 0$ in $\Omega \setminus \Omega_t$. We now introduce the discretized optimization problem $(\bar{\mathbf{P}}_\epsilon^{\alpha,\beta})$ as

$$\begin{aligned} (\bar{\mathbf{P}}_\epsilon^{\alpha,\beta}) \quad & -\langle B\mathbf{I}_S, \tilde{\mathbf{e}} \rangle + \alpha \langle \mathbf{I}_S, \mathbf{I}_S \rangle + \beta \|\mathbf{I}_S\|_1 \rightarrow \min_{\mathbf{I}_S \in \mathbb{R}^{S-1}} \\ \text{subject to} \quad & \omega_i |(B\mathbf{I}_S)_i| \leq \epsilon \end{aligned}$$

The existence (and potential uniqueness) of minimizers of the discretized optimization problem follows now directly from the above results since the regularity of finite element basis functions implies that the set

$$\mathcal{D}(\Gamma) = \left\{ \mathbf{I} = \sum_{i=1}^S I_i \phi_i \right\}$$

satisfies all assumptions needed. For the sake of brevity we do not discuss the issue of convergence of minimizers as $S \rightarrow \infty$, which can, e.g., be shown via Γ -convergence of the functionals involved.

4 Numerical Optimization

For numerical solution of the corresponding discretized problem we employ the alternating direction method of multipliers (ADMM) [5]. The ADMM is a variant of the *Augmented Lagrangian method*, a class for solving constrained optimization problems. The method combines important convergence properties (no strict convergence or finiteness is required) and the decomposability of the dual ascent method [5].

To solve the discretized optimization problem $(\bar{\mathbf{P}}_\epsilon^{\alpha,\beta})$, we substitute $B\mathbf{I}_S = \mathbf{y} \in \mathbb{R}^{3N}$ and $\mathbf{I}_S = \mathbf{z} \in \mathbb{R}^{S-1}$ and obtain the following Lagrangian $L_{\mu_1, \mu_2}(\mathbf{I}_S, \mathbf{y}, \mathbf{z}, \mathbf{p}_1, \mathbf{p}_2)$ which is to be minimized

$$\begin{aligned} L_{\mu_1, \mu_2}(\mathbf{I}_S, \mathbf{y}, \mathbf{z}, \mathbf{p}_1, \mathbf{p}_2) &= \alpha \langle \mathbf{z}, \mathbf{z} \rangle + \beta \|\mathbf{z}\|_1 + \frac{\mu_1}{2} \langle \mathbf{z} - \mathbf{I}_S, \mathbf{z} - \mathbf{I}_S \rangle + \langle \mathbf{z} - \mathbf{I}_S, \mathbf{p}_1 \rangle \\ &\quad - \langle \mathbf{y}, \tilde{\mathbf{e}} \rangle + \frac{\mu_2}{2} \langle \mathbf{y} - B\mathbf{I}_S, \mathbf{y} - B\mathbf{I}_S \rangle + \langle \mathbf{y} - B\mathbf{I}_S, \mathbf{p}_2 \rangle \\ &\text{subject to } \omega_i |\mathbf{y}_i| \leq \epsilon \end{aligned}$$

with $\mu_1, \mu_2 \in \mathbb{R}$ and $\mathbf{p}_1 \in \mathbb{R}^{S-1}, \mathbf{p}_2 \in \mathbb{R}^{3N}$ being the *augmented Lagrangian parameters* and the *dual variables*, respectively [5].

\mathbf{I}_S -step: Rearranging and neglecting terms without \mathbf{I}_S , putting the integrals together and expanding leads to a quadratic minimization problem

$$\begin{aligned} \frac{\mu_1}{2} (\langle \mathbf{I}_S^{k+1}, \mathbf{I}_S^{k+1} \rangle - 2 \langle \mathbf{z}^k, \mathbf{I}_S^{k+1} \rangle + \frac{2}{\mu_1} \langle \mathbf{I}_S^{k+1}, \mathbf{p}_1^k \rangle) \\ + \frac{\mu_2}{2} (-2 \langle \mathbf{y}^k, B\mathbf{I}_S^{k+1} \rangle + \langle B\mathbf{I}_S^{k+1}, B\mathbf{I}_S^{k+1} \rangle + \frac{2}{\mu_2} \langle B\mathbf{I}_S^{k+1}, \mathbf{p}_2^k \rangle) \end{aligned}$$

Differentiating with respect to \mathbf{I}_S^{k+1} and setting the equation system to be zero results in

$$\begin{aligned} (\mu_1 Id + \mu_2 B^{tr} B) \mathbf{I}_S^{k+1} - (\mu_1 \mathbf{z}^k - \mathbf{p}_1^k + \mu_2 B^{tr} \mathbf{y}^k - B^{tr} \mathbf{p}_2^k) &= 0 \\ \Rightarrow \mathbf{I}_S^{k+1} &= (\mu_1 Id + \mu_2 B^{tr} B)^{-1} (\mu_1 \mathbf{z}^k - \mathbf{p}_1^k + \mu_2 B^{tr} \mathbf{y}^k - B^{tr} \mathbf{p}_2^k) \end{aligned}$$

\mathbf{y} -step: Rearranging and neglecting terms and putting the integrals together results in

$$\begin{aligned} \frac{\mu_2}{2} \langle \mathbf{y}^{k+1} - B\mathbf{I}_S^{k+1} - \frac{1}{\mu_2} \mathbf{p}_2^k - \frac{1}{\mu_2} \tilde{\mathbf{e}}, \mathbf{y}^{k+1} - B\mathbf{I}_S^{k+1} - \frac{1}{\mu_2} \mathbf{p}_2^k - \frac{1}{\mu_2} \tilde{\mathbf{e}} \rangle \\ \text{subject to } \omega_i |\mathbf{y}_i| \leq \epsilon \end{aligned}$$

which can be solved analytically as follows

$$\mathbf{y}_i^{k+1} = \begin{cases} \frac{\epsilon}{\omega_i} \frac{(B\mathbf{I}_S^{k+1} + \frac{1}{\mu_2} \mathbf{p}_2^k + \frac{1}{\mu_2} \tilde{\mathbf{e}})_i}{|(B\mathbf{I}_S^{k+1} + \frac{1}{\mu_2} \mathbf{p}_2^k + \frac{1}{\mu_2} \tilde{\mathbf{e}})_i|}, & \text{if } |(B\mathbf{I}_S^{k+1} + \frac{1}{\mu_2} \mathbf{p}_2^k + \frac{1}{\mu_2} \tilde{\mathbf{e}})_i| > \frac{\epsilon}{\omega_i} \\ (B\mathbf{I}_S^{k+1} + \frac{1}{\mu_2} \mathbf{p}_2^k + \frac{1}{\mu_2} \tilde{\mathbf{e}})_i, & \text{otherwise} \end{cases}$$

\mathbf{z} -step: Rearranging the terms, leaving out the terms without \mathbf{z} and putting the integrals together leads to

$$\begin{aligned} &\alpha \langle \mathbf{z}^{k+1}, \mathbf{z}^{k+1} \rangle + \beta \left\| \mathbf{z}^{k+1} \right\|_1 + \frac{\mu_1}{2} \langle \mathbf{z}^{k+1} - \mathbf{I}_S^{k+1}, \mathbf{z}^{k+1} - \mathbf{I}_S^{k+1} \rangle + \langle \mathbf{z}^{k+1} - \mathbf{I}_S^{k+1}, \mathbf{p}_1^k \rangle \\ &= \alpha \langle \mathbf{z}^{k+1}, \mathbf{z}^{k+1} \rangle \\ &+ \underbrace{\langle \sqrt{\frac{\mu_1}{2}} Id \mathbf{z}^{k+1} - \sqrt{\frac{\mu_1}{2}} \mathbf{I}_S^{k+1} - \frac{1}{\sqrt{2\mu_1}} \mathbf{p}_1^k + \frac{1}{\sqrt{2\mu_1}} \beta, \sqrt{\frac{\mu_1}{2}} Id \mathbf{z}^{k+1} - \sqrt{\frac{\mu_1}{2}} \mathbf{I}_S^{k+1} - \frac{1}{\sqrt{2\mu_1}} \mathbf{p}_1^k + \frac{1}{\sqrt{2\mu_1}} \beta \rangle}_{:= \tilde{Id}} \end{aligned}$$

Algorithm 1 Algorithm for the discretized minimization problem $(\bar{\mathbf{P}}_\epsilon^{\alpha,\beta})$

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1: Input:  $B, \epsilon, \mu_1, \mu_2, \alpha, \beta, \omega, \tilde{\mathbf{e}}, \mathbf{I}_{prev}, \mathbf{I}_S^0, \mathbf{p}_1^0, \mathbf{p}_2^0, \mathbf{z}^0, \mathbf{y}^0, N, TOL$ 
2:  $k = 0$ 
3: while  $k < 3$  or  $\|\mathbf{I}_S^k - \mathbf{I}_{prev}\| > TOL$  do
4:    $\mathbf{I}_{prev} = \mathbf{I}_S^k$ 
5:    $\mathbf{I}_S^{k+1} = (\mu_1 Id + \mu_2 B^{tr} B)^{-1} (\mu_1 \mathbf{z}^k - \mathbf{p}_1^k + \mu_2 B^{tr} \mathbf{y}^k - B^{tr} \mathbf{p}_2^k)$ 
6:   for  $i = 1, \dots, 3N$  do
7:     if  $|(B\mathbf{I}_S^{k+1} + \frac{1}{\mu_2} \mathbf{p}_2^k + \frac{1}{\mu_2} \tilde{\mathbf{e}})_i| > \frac{\epsilon}{\omega_i}$  then
8:        $\mathbf{y}_i^{k+1} = \frac{\epsilon}{\omega_i} \frac{(B\mathbf{I}_S^{k+1} + \frac{1}{\mu_2} \mathbf{p}_2^k + \frac{1}{\mu_2} \tilde{\mathbf{e}})_i}{|(B\mathbf{I}_S^{k+1} + \frac{1}{\mu_2} \mathbf{p}_2^k + \frac{1}{\mu_2} \tilde{\mathbf{e}})_i|}$ 
9:     else
10:       $\mathbf{y}_i^{k+1} = (B\mathbf{I}_S^{k+1} + \frac{1}{\mu_2} \mathbf{p}_2^k + \frac{1}{\mu_2} \tilde{\mathbf{e}})_i$ 
11:    end if
12:  end for
13:   $\mathbf{z}^{k+1} = (\tilde{I}^{tr} \tilde{I}d + \alpha Id)^{-1} \tilde{I}^{tr} (\sqrt{\frac{\mu_1}{2}} \mathbf{I}_S^{k+1} + \frac{1}{\sqrt{2\mu_1}} \mathbf{p}_1^k - \frac{1}{\sqrt{2\mu_1}} \beta)$ 
14:   $\mathbf{p}_1^{k+1} = \mu_1 (\mathbf{p}_1^k + \mathbf{I}_S^{k+1} - \mathbf{z}^{k+1})$ 
15:   $\mathbf{p}_2^{k+1} = \mu_2 (\mathbf{p}_2^k + B\mathbf{I}_S^{k+1} - \mathbf{y}^{k+1})$ 
16:   $k = k + 1$ 
17: end while
18:  $\delta = \frac{4\epsilon}{\|\mathbf{I}_S^{k+1}\|_{\mathcal{M}(\Gamma)}}$ 
19: return  $\mathbf{I}_S^{k+1}, \delta, k, \|\mathbf{I}_S^{k+1}\|_{\mathcal{M}(\Gamma)}$ 

```

Table 1: Tangential target vector $\tilde{\mathbf{e}}$: Averaged (over 924 targets) scaled threshold value δ , the number of iterations k and the scaling factor $\|\mathbf{I}\|_{\mathcal{M}(\Gamma)}$ for tangential target vectors $\tilde{\mathbf{e}}$ and different input values ϵ .

$\epsilon [Am^{-2}]$	0.0001	0.0005	0.001	0.005	0.01
$\delta [Am^{-2}]$	0.00332	0.0085	0.0154	0.0175	0.0208
Iterations k	132	53	33	203	143
$\ \mathbf{I}\ _{\mathcal{M}(\Gamma)}$	120.15	233.96	352.279	1312.2	1919.93

The solution to this equation is given as

$$\mathbf{z}^{k+1} = (\tilde{I}^{tr} \tilde{I}d + \alpha Id)^{-1} \tilde{I}^{tr} (\sqrt{\frac{\mu_1}{2}} \mathbf{I}_S^{k+1} + \frac{1}{\sqrt{2\mu_1}} \mathbf{p}_1^k - \frac{1}{\sqrt{2\mu_1}} \beta)$$

Dual update: Finally, the dual variables are updated

$$\begin{aligned} \mathbf{p}_1^{k+1} &= \mu_1 (\mathbf{p}_1^k + \mathbf{I}_S^{k+1} - \mathbf{z}^{k+1}) \\ \mathbf{p}_2^{k+1} &= \mu_2 (\mathbf{p}_2^k + B\mathbf{I}_S^{k+1} - \mathbf{y}^{k+1}) \end{aligned}$$

Algorithm 1 depicts an overview of the optimization steps for the numerical solution of the discretized problem $(\bar{\mathbf{P}}_\epsilon^{\alpha,\beta})$.

5 Results and Discussion

We generated a highly realistic geometry-adapted six-compartment (skin, skull compacta, skull spongiosa, CSF, gray and white matter) finite element head model from a T1- and a T2-weighted magnetic resonance image (MRI). For the compartments skin, skull compacta, skull spongiosa, CSF and gray matter we employed conductivity values $\sigma = 0.43 \text{ S m}^{-1}$, 0.007 S m^{-1} , 0.025 S m^{-1} , 1.79 S m^{-1} and 0.33 S m^{-1} , respectively [15, 21, 25]. For the modeling of the white matter anisotropy, a diffusion tensor MRI was used and the effective medium approach was applied. The effective medium approach assumes a linear relationship between the effective electrical conductivity tensor and the effective water diffusion tensor in white matter [24], resulting in a mean conductivity value $\sigma = 0.14 \text{ S m}^{-1}$ for the white matter compartment. As the current density amplitudes in the skin and CSF compartments are much stronger when compared to the brain compartments [25], we only visualized the current densities in the brain to enable best visibility of the cortical current flow pattern. The software package SCIRun was used for visualization [7].

Using this highly realistic volume conductor model we comprehensively examine the optimized current densities in the brain with regard to focality, target intensity and orientation. Firstly, the maximal current density in non-target regions is investigated for the discretized optimization problem $(\bar{\mathbf{P}}_\epsilon^{\alpha,\beta})$ and four target vectors are used to calculate optimized stimulation protocols. For all simulations, the target area Ω_t always consists of the elements corresponding to the target vectors and only the volume conductor elements in the brain are used for optimization, i.e., $\omega = 1$ only in the brain compartments and $\omega \ll 1$ in the target region and in the CSF, skin and skull compartments.

In order to investigate the current flow field that is induced by an optimized standard bipolar electrode montage, we use a maximum two electrode (M2E) approach. This approach stimulates only the main positive (anode) and the main negative electrode (cathode) of the L1R optimized stimulation protocols with a total current of 1 mA. In order to quantify the optimized current flow fields, we calculate the current densities in the direction of the target vectors (CD_t) and the percentage of current density that is oriented parallel to the target vector (PAR), as shown in columns 4 and 5 in Table 3, respectively.

5.1 Maximal current density in non-target regions

In this section, the L1R approximated discretized optimization problem $(\bar{\mathbf{P}}_\epsilon^{0,\beta})$ with $\beta = 0.001$ is used to calculate optimized stimulation protocols for a set of 924 tangential (parallel to the inner skull surface) and radial (perpendicular to the inner skull surface) target vectors and Theorem 3 is applied to estimate the averaged maximal current density in non-target regions as shown in Tables 1 and 2. Furthermore, the number of iterations until a minimum was found and the scaling factor $\|\mathbf{I}\|_{\mathcal{M}(T)}$ is depicted. As can be seen in the tables, for the threshold value $\epsilon = 0.001 \text{ A m}^{-2}$, the averaged maximal current density in non-target regions δ is weak and the number of iterations k until a minimum was found is lowest. For this reason, a threshold value of $\epsilon = 0.001 \text{ A m}^{-2}$ is thus used in this study as it allows safe and well-targeted stimulation and fast and robust computation of the stimulation protocol.

5.2 Mainly tangential target vector

Figure 2 displays the optimized current densities (for better visibility, we used a different scaling) and the corresponding stimulation protocols (same scaling) for a mainly tangential target vector as shown in Figures 2-A1 and -A2. As can be seen in Figures 2-B1 and 2-C1,

Table 2: Radial target vector $\tilde{\mathbf{e}}$: Averaged (over 924 targets) scaled threshold value δ , the number of iterations k and the scaling factor $\|\mathbf{I}\|_{\mathcal{M}(\Gamma)}$ for radial target vectors $\tilde{\mathbf{e}}$ and different input values ϵ .

$\epsilon [Am^{-2}]$	0.0001	0.0005	0.001	0.005	0.01
$\delta [Am^{-2}]$	0.0043	0.0114	0.015	0.023	0.025
Iterations k	134	36	35	68	118
$\ \mathbf{I}\ _{\mathcal{M}(\Gamma)}$	92.03	176.08	267.06	887.08	1597.73

the optimized current flow fields using the L2R and L1R approaches, respectively, show high focality and maximal current densities can be observed in the target region. While the L2R and L1R approaches lead to target current densities of 0.022 A m^{-2} and 0.038 A m^{-2} (Table 3, second column), current densities in non-target brain regions are rather weak (Figures 2-B1 and -C1). Overall, due to the rather widespread applied current pattern at the fixed electrodes (Figure 2-B2), the L2R optimized current flow field (Figure 2-B1) has smaller amplitude when compared to the L1R one (Figure 2-C1). On the other hand, the L1R stimulation protocol (Figure 2-C2) shows high focality with mainly two active electrodes, while only very weak compensating currents are injected at the neighboring electrodes. The M2E approach results in higher target current densities of 0.071 A m^{-2} (Table 3, second column). However, using the M2E approach, relatively strong current densities can also be noted in non-target regions, especially in pyramidal tract and deeper white matter regions (Figure 2-D1).

With a PAR value of 86.4, 86.8 and 85.9 for L2R, L1R and M2E (Table 3, fifth column), the current densities of all three approaches are mainly oriented parallel to the target vector, leading to CD_t values, i.e., current densities along the target direction, of 0.019, 0.033 and 0.061 A m^{-2} , resp. (Table 3, fourth column). While the CD_t values between L1R and M2E are thus less than a factor of 2 different, the averaged current density amplitudes in non-target regions is about 5.3 times higher when using the M2E approach (Table 3, third column). The L1R optimized current flow field thus shows significantly higher focality and also slightly better parallelity to the target vector in comparison to the bipolar electrode montage M2E. However, if no multi-channel tDCS stimulator is available, the M2E approach provides an optimized bipolar electrode montage for a mainly tangential target vector.

5.3 Mainly radial target vector

The mainly radially oriented target is shown in Figures 3-A1 and -A2. Figures 3-B1 and 3-C1 depict the optimized current densities for the L2R and L1R approaches, resp.. As shown in Table 3 (Column 2), with a value of 0.045 A m^{-2} , the target current density for the L1R approach is more than a factor of 1.7 times stronger than with the L2R approach (0.026 A m^{-2}). Non-target regions show only weak current densities (Figures 3-B1 and -C1). With a value of 0.063 A m^{-2} , the M2E approach yields the largest target intensity (Table 3, second column). However, for this approach, the maximal current density in the brain does not occur in the target region, but on a neighboring gyrus in between the stimulating electrodes and in mainly tangential direction (Figure 3-D1). Moreover, the M2E optimized current density shows again an overall much lower focality than the L2R and L1R current flow fields.

The L2R stimulation protocol (Figure 3-B2) consists of an anode above the target, sur-

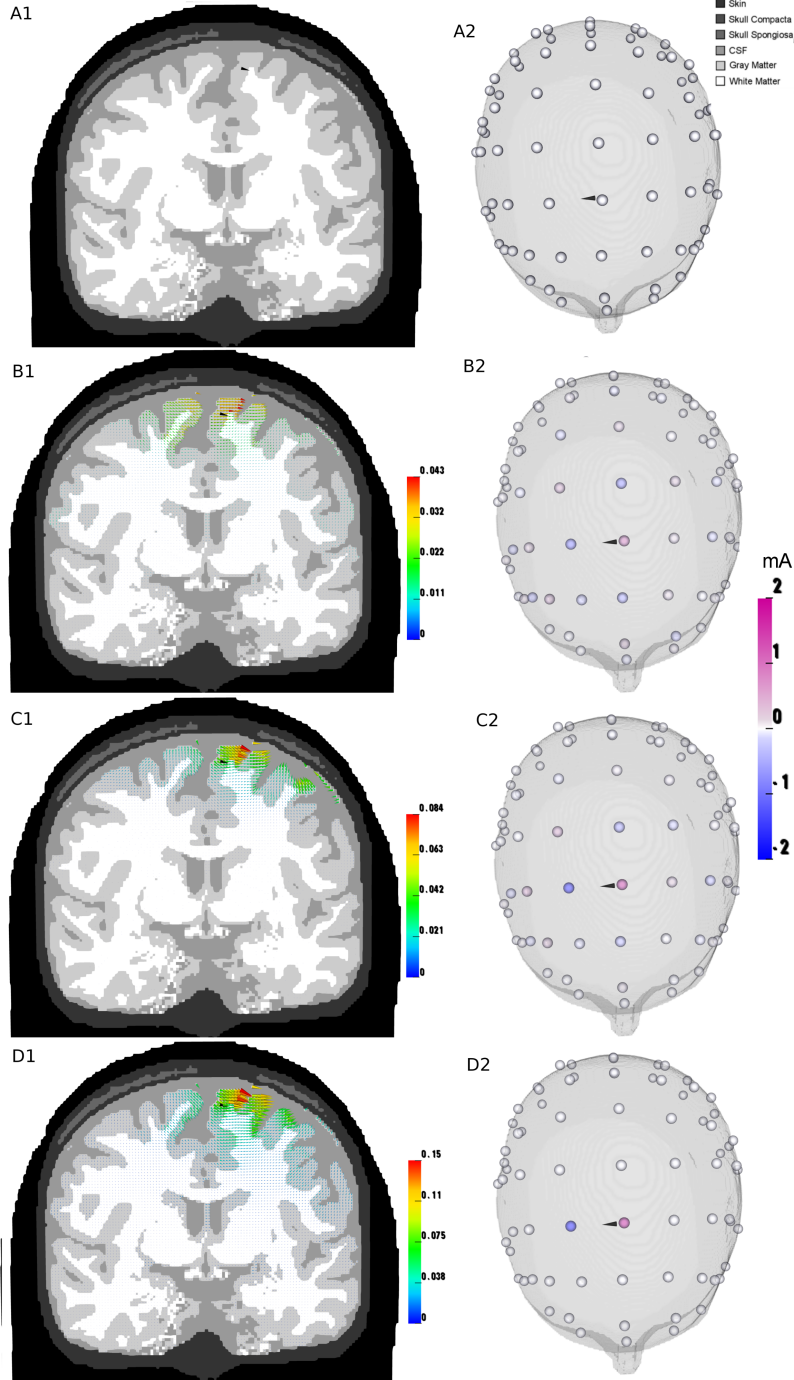


Figure 2: A mainly tangential target vector (Figures -A1 and -A2): Figures -B -C and -D present optimization results for the L2R, L1R and M2E approach, respectively. The optimized current densities in the brain compartment (note the different scaling) and the corresponding stimulation protocols (same scaling) are shown in Figures -1 and -2, respectively.

rounded by four cathodes and a ring of very weak positive currents at the second neighboring electrodes, a distribution which might be best described by a sinc-function. As can be seen in Figure 3-C2, the L1R stimulation protocol is mainly composed of a main

Table 3: Quantification of optimized current density. The averaged current density in the target area (CD_a , second column), the averaged current density in non-target regions (third column), the inner product of current density and target vector (CD_t , fourth column) and the percentage of current density that is oriented parallel to the target vector (PAR, fifth column) is displayed for different target vectors and methods (first column).

Target	$\frac{\int_{\Omega_t} \mathbf{BI}_S d\mathbf{x}}{ \Omega_t }$	$\frac{\int_{\Omega \setminus \Omega_t} \mathbf{BI}_S d\mathbf{x}}{ \Omega \setminus \Omega_t }$	$\frac{\int_{\Omega} \langle \mathbf{BI}_S, \mathbf{e} \rangle d\mathbf{x}}{ \Omega_t }$	PAR = $\frac{CD_t}{CD_a}$
		$[Am^{-2}]$		$[\%]$
tangential L2R	0.022	0.00144	0.019	86.4
tangential L1R	0.038	0.00151	0.033	86.8
tangential M2E	0.071	0.0080	0.061	85.9
radial L2R	0.026	0.00064	0.025	96.1
radial L1R	0.045	0.00071	0.043	95.5
radial M2E	0.063	0.0074	0.048	76.2
patch L2R	0.025	0.00147	0.022	88.0
patch L1R	0.037	0.00157	0.033	89.1
patch M2E	0.071	0.0080	0.062	87.3
deep L2R	0.015	0.00345	0.013	86.7
deep L1R	0.019	0.00249	0.018	94.7
deep M2E	0.052	0.01477	0.049	94.2

positive current at the electrode above the target region and four return currents applied to the surrounding electrodes.

The L2R and L1R optimized current flow fields show high directional agreement with the target vector \mathbf{e} (PAR value above 95 %), with the L2R slightly outperforming the L1R approach (Table 3, fifth column). With a PAR value of only 76.2% the current flow field in the M2E model shows much less directional agreement with the target vector. This results in CD_t values of 0.025, 0.043 and 0.048 A m⁻² for the L2R, L1R and M2E approaches, resp.. In order to obtain higher PAR values for the M2E approach, i.e., higher current densities along the target direction, the distance between anode and cathode might be enlarged, in line with Dmochowski and colleagues [8] who reported that the optimal bipolar electrode configuration for a radial target vector consists of an electrode placed directly over the target with a distant return electrode. Another interesting bipolar electrode arrangement for a radial target vector might consist of an anode over the target and a cathodal ring around the anode.

5.4 Extended mainly tangential target vector region

In this section, an extended target area of 3 mm × 1 mm × 1 mm is used for current density optimization. The target area is centered around the location of the superficial target vector that was also used in Section 5.2 and the corresponding target vectors are selected to be mainly tangentially oriented (Figures 4-A1 and 4-A2). As can be seen in Figures 4-B1 and 4-C1, the optimized current flow fields of the L2R and L1R approaches show high focality. L2R and L1R yield an averaged target intensity of 0.025 A m⁻² and 0.037 A m⁻², resp. (Table 3, second column). Current density is not restricted to but

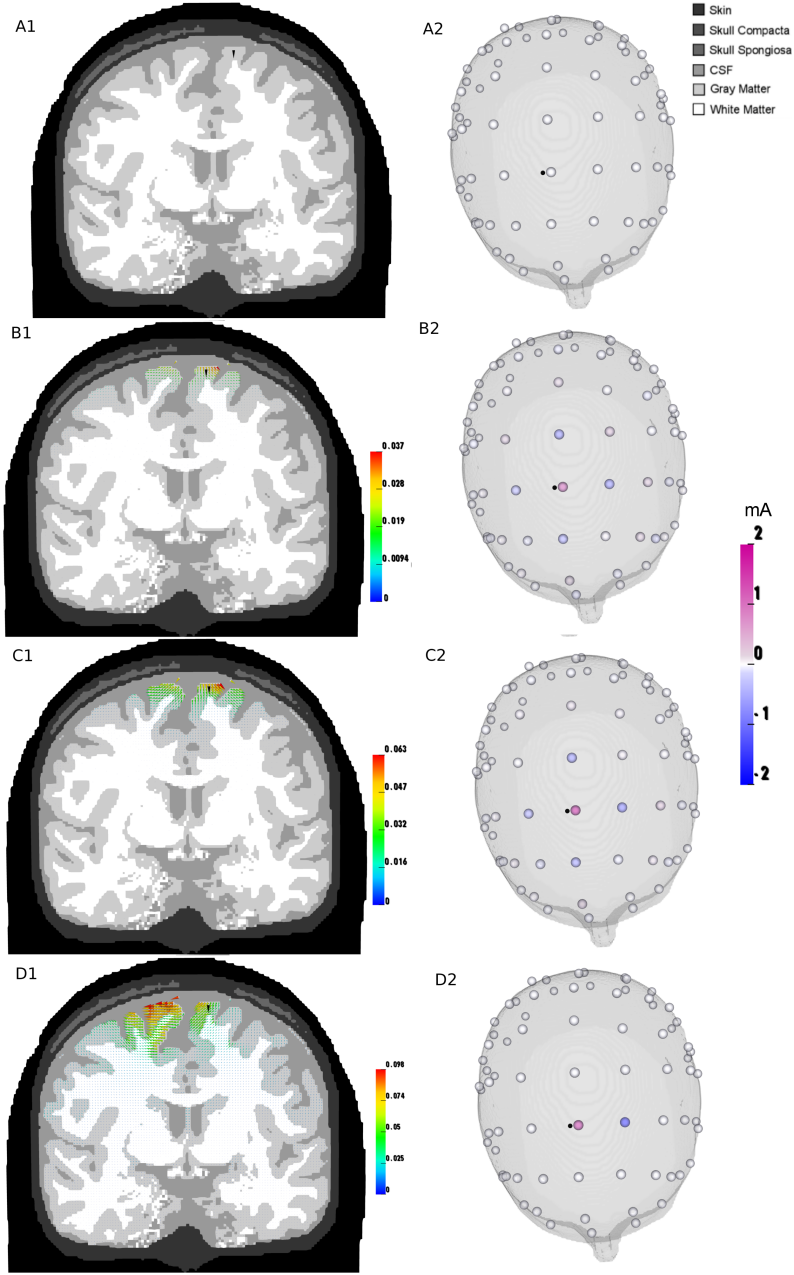


Figure 3: A mainly radial target vector (Figures -A1 and -A2): Figures -B -C and -D present optimization results for the L2R, L1R and M2E approach, respectively. The optimized current densities in the brain compartment (note the different scaling) and the corresponding stimulation protocols (same scaling) are shown in Figures -1 and -2, respectively.

focused to the target area, especially for the L2R approach (Figure 4-B1). In comparison to the superficial tangential target vector of Section 5.2, the L1R optimized averaged current density in the target area is decreased by about 3 % (from 0.038 A m^{-2} to 0.037 A m^{-2}) and the optimized stimulation protocols are also very similar. Because the main two electrodes are taken from the L1R optimization, this implies that also the M2E stimulation protocol remains constant to the stimulation protocol from Section 5.2. In this way, the M2E

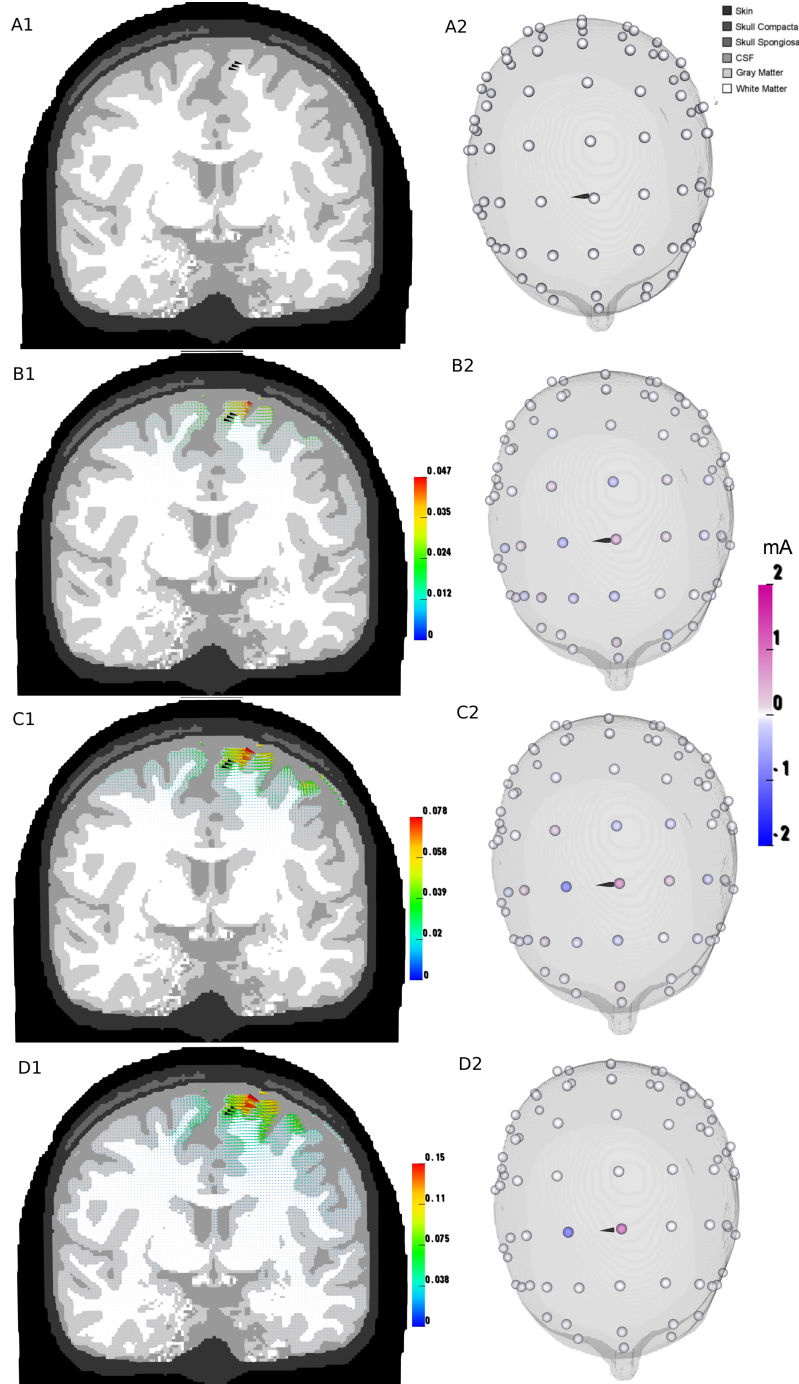


Figure 4: An extended target region consisting of 3 tangential target vectors (Figures -A1 and -A2): Figures -B -C and -D present optimization results for the L2R, L1R and M2E approach, respectively. The optimized current densities in the brain compartment (note the different scaling) and the corresponding stimulation protocols (same scaling) are shown in Figures -1 and -2, respectively.

approach yields an averaged target intensity of 0.071 A m^{-2} (Table 3, second column). With averaged *PAR* values of 88.0, 89.1 and 87.3 (Table 3, fifth column), the current densities are mainly oriented parallel to the target vectors with L1R performing best.

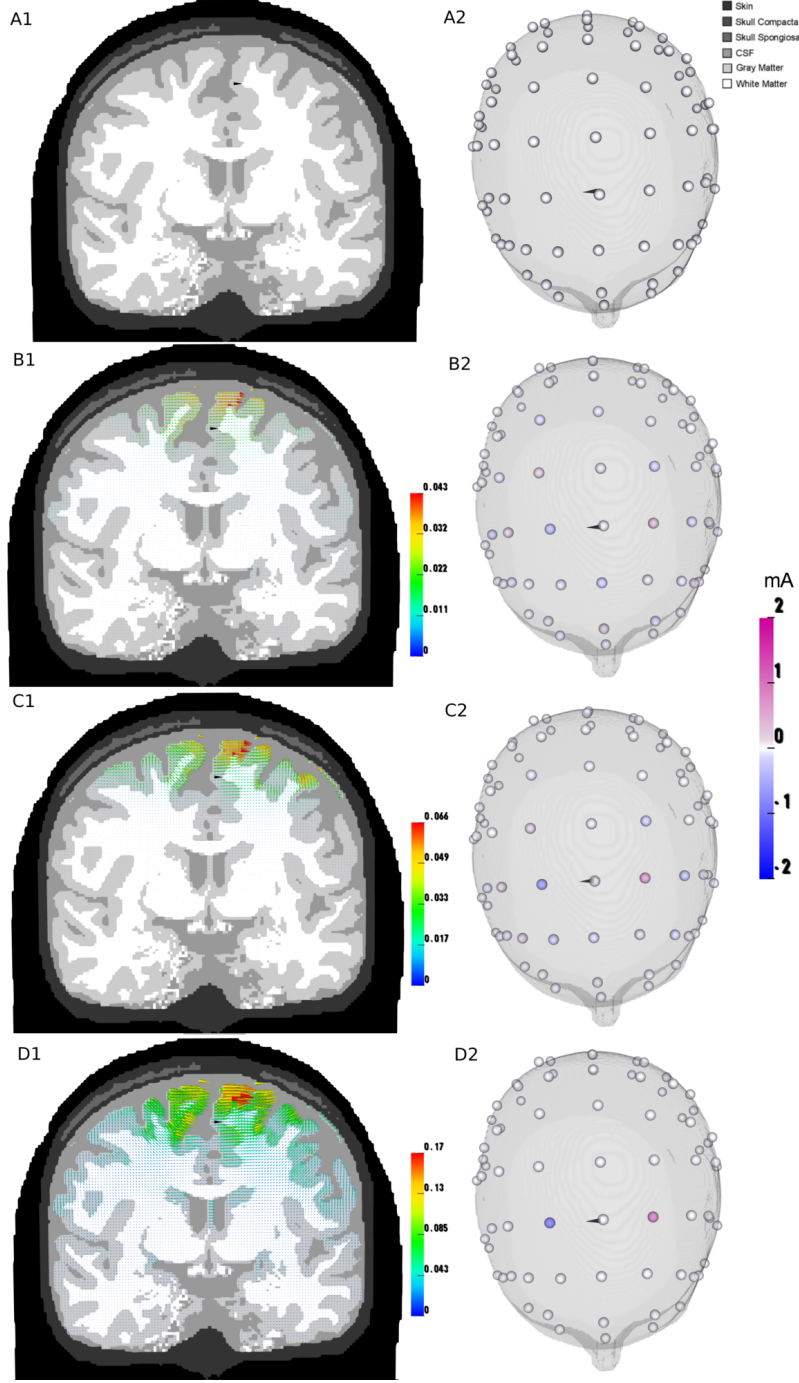


Figure 5: A deeper target vector (Figures -A1 and -A2): Figures -B -C and -D present optimization results for the L2R, L1R and M2E approach, respectively. The optimized current densities in the brain compartment (note the different scaling) and the corresponding stimulation protocols (same scaling) are shown in Figures -1 and -2, respectively.

The averaged current flow field intensity along the target direction is 0.022, 0.033 and 0.062 A m^{-2} for the L2R, L1R and M2E approaches, resp. (Table 3, fourth column). However, for M2E also non-target regions reach significant current densities, as clearly shown in Figure 4-D1. The averaged current density amplitudes in non-target regions is

0.00157 and 0.0080 A m⁻² for the L1R and M2E approaches (Table 3, third column). The L1R optimized current flow field thus shows a factor of 5.1 higher focality in comparison to bipolar electrode montage M2E. However, the M2E approach provides an optimized bipolar electrode montage for an extended target area of tangential target vectors.

5.5 Deep and tangential target vector

In the last simulation scenario, we investigate optimization for a deeper and mainly tangentially oriented target vector as shown in Figures 5-A1 and -A2. Figures 5-B1 and -C1 depict the optimized current density distributions when using L2R and L1R for optimization, resp.. For those approaches, the target current densities are 0.015 and 0.019 A m⁻², resp.. With a value of 0.052 A m⁻², which is more than 2.7 times the L1R value, the largest target intensity is, however, achieved with the M2E approach (Table 3, second column). CD_t values of 0.013, 0.018 and 0.049 A m⁻² lead to PAR values of 86.7, 94.7 and 94.2 for the L2R, L1R and M2E approaches (Table 3, fourth and fifth column). The target current densities are thus for all three approaches oriented mainly parallel to the target vector.

The L2R and L1R stimulation protocols show high focality with mainly two active electrodes, while only weak compensating currents are injected at the neighboring electrodes (Figures 2-B2 and -C2). Similar to Section 5.2, the compensating currents are stronger when using the L2R optimization procedure, leading to weaker target brain current densities as compared to the L1R stimulation. In order to enable current density to penetrate into deeper brain regions, the distance between the two main stimulating electrodes is larger when compared to the superficial mainly tangential target vector from Section 5.2, i.e., the electrode above the target region is not used for stimulation, while a more distant electrode is used as anode.

For all three approaches, strongest current density amplitudes in the brain compartment always occur at the CSF/brain boundary above the target region (Figures 5-B1,-C1 and -D1). This is due to the fact that the potential field $\nabla\Phi$ satisfies the maximum principle for harmonic functions which states that a non-constant function always attains its maximum at the boundary of the domain [12, Theorem 14.1]. Nevertheless, in average over all non-target regions, with a value of 0.01477 A m⁻² for M2E, the L2R (0.00345 A m⁻²) and L1R (0.00249 A m⁻²) optimized current flow fields show a factor of about 4.3 and 5.9 times lower current densities, resp. (Table 3, third column). Overall, L2R and L1R thus have a much higher focality, which can also easily be seen in Figures 5-B1,-C1 and -D1. However, if no multi-channel tDCS device is available, the M2E approach provides an optimized bipolar electrode arrangement for a deep and tangential target vector.

6 Conclusion and Outlook

A novel optimization approach for safe and well-targeted multi-channel transcranial direct current stimulation has been proposed. Existence of at least one minimizer and residual and objective convergence results have been proven for the proposed optimization methods. For discretization of the respective minimization problems the finite element method was employed and the existence of at least one minimizer to the discretized optimization problems have been shown. For numerical solution of the corresponding discretized problem we employed the alternating direction method of multipliers. A highly-realistic six-compartment head model with white matter anisotropy was generated and optimized current density distributions were calculated and evaluated for a mainly tangential and a

mainly radial target vector at superficial locations, an extended target area and a deeper mainly tangential target vector. The numerical results revealed that, while all approaches fulfilled the patient safety constraint, the optimized current flow fields show significantly higher focality and, with the exception of the L2R for the deep target, higher directional agreement to the target vector in comparison to standard bipolar electrode montages. The higher directional agreement is especially distinct for the radial target vector. In all test cases, because of a more widespread distribution of injected and extracted surface currents, the L2R optimization procedure ($\bar{\mathbf{P}}_e^{\alpha,0}$) led to relatively weak current densities in the brain compartment. The L1R optimized current density distribution along the target direction was in all test cases stronger than the L2R one and might thus be able to induce more significant stimulation effects. The stimulation will thus enhance cortical excitability especially in the target regions, while it will as good as possible prevent too strong excitability changes in non-target regions.

We were able to demonstrate that the M2E approach provides optimized bipolar electrode montages as long as the target is mainly tangentially oriented. For radial targets, the M2E approach was unsatisfactory, an optimal bipolar electrode configuration might then consist of a small electrode placed directly above the target region with a distant return electrode or a small electrode over the target encircled by a ring return electrode, as proposed in [8].

A further application for the optimization method is transcranial magnetic stimulation (TMS). TMS uses externally generated magnetic fields to induce electrical currents to the underlying brain tissue [13]. Because there is no safety limit for the total currents applied to the stimulating coils but a safety-threshold for painful muscle twitching [13], the constrained optimization problem for multi-coil TMS is given as

$$\begin{aligned}
(\mathbf{P}_{\text{TMS}}) \quad & - \int_{\Omega_t} \langle \sigma \nabla \Phi, \mathbf{e} \rangle d\mathbf{x} \rightarrow \min \\
& \text{subject to} \quad \omega |\sigma \nabla \Phi| \leq E_M \\
& \nabla \cdot \sigma \nabla \Phi = -\nabla \cdot \sigma \frac{\partial \mathbf{A}(\mathbf{x}, t)}{\partial t} \quad \text{in } \Omega \\
& \langle \sigma \nabla \Phi, \mathbf{n} \rangle = -\langle \sigma \frac{\partial \mathbf{A}(\mathbf{x}, t)}{\partial t}, \mathbf{n} \rangle \quad \text{on } \partial \Gamma \\
& \Phi = 0 \quad \text{on } \Gamma_D
\end{aligned}$$

with $\mathbf{A}(\mathbf{x}, t)$ being the time-dependent magnetic vector potential and $E_M = 450 \text{ V m}^{-1}$ being the threshold for painful muscle twitching [13]. The existence of at least one minimizer to the constrained optimization problem for TMS directly follows from Theorem 2. Because the optimization method can be applied for both brain stimulation modalities, a combined tDCS and TMS optimization might outperform single modality tDCS or TMS optimizations, similar to what was shown for electro- (EEG) and magnetoencephalography (MEG) [1, 2]. While tCS is able to stimulate a radially oriented target, TMS is mainly not (like MEG is hardly able to detect radial sources [1, 2]). Possible applications of combined tDCS and TMS multi-channel and multi-coil optimization might thus be an improved stimulation of target regions containing both radial and tangential orientations or of deeper target regions. In order to induce action potentials in deeper target regions, the induced current density should exceed the threshold for neuronal depolarization of 150 V m^{-1} [13]. On the other hand, the threshold for painful muscle twitching of 450 V m^{-1} must be kept [13]. The combination of the optimized tDCS and TMS current density fields might lead to higher current densities in the target and simultaneously reduced current density amplitudes in non-target regions.

A Convergence analysis

In this section we show residual and objective convergence results for the simplified optimization problem (\mathbf{P}_ϵ) . We mainly follow the work of Boyd and colleagues [5].

An admissible set $\mathcal{D}^{ad}(\Gamma) := \{\tilde{\mathbf{J}} \in \mathcal{D}(\Gamma) \mid \omega |A\tilde{\mathbf{J}}| \leq \epsilon\} \subset \mathcal{D}(\Gamma)$ is introduced which ensures that the state constraint is always fulfilled for

$$-\int_{\Omega} \langle A\mathbf{J}, \tilde{\mathbf{e}} \rangle d\mathbf{x} \rightarrow \min_{\mathbf{J} \in \mathcal{D}^{ad}(\Gamma)}$$

This minimization problem is similar to the simplified optimization problem (\mathbf{P}_ϵ) . Then, the augmented Lagrangian reads

$$L_\mu(\mathbf{J}, \mathbf{z}, \mathbf{p}) = -\int_{\Omega} \langle \mathbf{z}, \tilde{\mathbf{e}} \rangle d\mathbf{x} + \int_{\Omega} (A\mathbf{J} - \mathbf{z})\mathbf{p} d\mathbf{x} + \frac{\mu}{2} \|A\mathbf{J} - \mathbf{z}\|_2^2$$

with μ and \mathbf{p} being the augmented Lagrangian parameter and the dual variable, respectively [5]. We assume that the unaugmented Lagrangian L_0 has a saddle point and that the function

$$g(\mathbf{z}) = -\int_{\Omega} \langle \mathbf{z}, \tilde{\mathbf{e}} \rangle d\mathbf{x}$$

is closed, proper and convex. Furthermore, we define

$$\mathbf{q}^* = \inf \left\{ -\int_{\Omega} \langle \mathbf{z}, \tilde{\mathbf{e}} \rangle d\mathbf{x} \mid A\mathbf{J} - \mathbf{z} = 0 \right\}$$

and

$$\mathbf{q}^{k+1} = -\int_{\Omega^*} \langle \mathbf{z}^{k+1}, \tilde{\mathbf{e}} \rangle d\mathbf{x}$$

In order to show residual convergence and objective convergence for the simplified optimization problem, we introduce three inequalities

- E1: $\mathbf{q}^* - \mathbf{q}^{k+1} \leq (\mathbf{p}^*)^{tr} \mathbf{r}^{k+1}$
- E2: $\mathbf{q}^{k+1} - \mathbf{q}^* \leq -(\mathbf{p}^{k+1})^{tr} \mathbf{r}^{k+1} + \mu(\mathbf{z}^{k+1} - \mathbf{z}^k)^{tr} (-\mathbf{r}^{k+1} - (\mathbf{z}^{k+1} - \mathbf{z}^*))$
- E3: $V^{k+1} \leq V^k - \mu \|\mathbf{r}^{k+1}\|_2^2 - \mu \|\mathbf{z}^{k+1} - \mathbf{z}^k\|_2^2$

with $V^k := \frac{1}{\mu} \|\mathbf{p}^k - \mathbf{p}^*\|_2^2 + \mu \|\mathbf{z}^k - \mathbf{z}^*\|_2^2$ and $\mathbf{p}^* = \lim_{k \rightarrow \infty} \mathbf{p}^{k+1}$. The derivation of the inequalities require only minor changes of the standard proof given in [5].

The residual convergence $\mathbf{r}^{k+1} = A\mathbf{J}^{k+1} - \mathbf{z}^{k+1} \rightarrow 0$ for $k \rightarrow \infty$ directly follows from Inequality E3: As both $\|\mathbf{r}^{k+1}\|_2^2$ and $\|\mathbf{z}^{k+1} - \mathbf{z}^k\|_2^2$ are positive it follows that V^k are positive and $V^k \leq V^0$ which implies that both \mathbf{p}^k and \mathbf{z}^k are bounded. Summing up the V^k leads to

$$\mu \left(\sum_{k=0}^{\infty} \left\| \mathbf{r}^{k+1} \right\|_2^2 + \left\| \mathbf{z}^{k+1} - \mathbf{z}^k \right\|_2^2 \right) \leq V^0 + \mu \left(\sum_{k=0}^{\infty} \left\| \mathbf{r}^{k+1} \right\|_2^2 + \left\| \mathbf{z}^{k+1} - \mathbf{z}^k \right\|_2^2 \right) \leq V^0$$

which implies $\mathbf{r}^{k+1} \rightarrow 0$ and $\mathbf{z}^{k+1} - \mathbf{z}^k \rightarrow 0$ for $k \rightarrow \infty$.

As \mathbf{p}^{k+1} is bounded and both \mathbf{r}^{k+1} and $\mathbf{z}^{k+1} - \mathbf{z}^k$ converge to zero, the objective convergence $\lim_{k \rightarrow \infty} \mathbf{q}^{k+1} = \mathbf{q}^*$ directly follows from Inequalities E2 and E1.

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