

Johnson, C. R. “ Numerical Methods for Bioelectric Field Problems.”  
*The Biomedical Engineering Handbook: Second Edition.*  
Ed. Joseph D. Bronzino  
Boca Raton: CRC Press LLC, 2000

# 12

## Numerical Methods for Bioelectric Field Problems

---

- 12.1 [Problem Formulation](#)
- 12.2 [Model Construction and Mesh Generation](#)
- 12.3 [Numerical Methods](#)
  - Approximation Techniques • The Galerkin Method • The Finite-Difference Method • The Finite-Element Method • Application of the FE Method for 3D Domains • The Boundary-Element Method • Solution Methods and Computational Considerations • Comparison of Methods
- 12.4 [Adaptive Methods](#)
  - Convergence of a Sequence of Approximate Solutions • Energy Norms

Christopher R. Johnson  
*University of Utah*

Computer modeling and simulation continue to grow more important to the field of bioengineering. The reasons for this growing importance are manyfold. First, mathematical modeling has been shown to be a substantial tool for the investigation of complex biophysical phenomena. Second, since the level of complexity one can model parallels existing hardware configurations, advances in computer architecture have made it feasible to apply the computational paradigm to complex biophysical systems. Hence, while biologic complexity continues to outstrip the capabilities of even the largest computational systems, the computational methodology has taken hold in bioengineering and has been used successfully to suggest physiologically and clinically important scenarios and results.

This chapter provides an overview of numerical techniques that can be applied to a class of bioelectric field problems. Bioelectric field problems are found in a wide variety of biomedical applications that range from single cells [1], to organs [2], up to models that incorporate partial to full human structures [3,4,5]. I describe some general modeling techniques that will be applicable, in part, to all the aforementioned problems. I focus this study on a class of bioelectric volume conductor problems that arise in electrocardiography and electroencephalography.

I begin by stating the mathematical formulation for a bioelectric volume conductor, continue by describing the model construction process, and follow with sections on numerical solutions and computational considerations. I concluded with a section on error analysis coupled with a brief introduction to adaptive methods.

## 12.1 Problem Formulation

As noted in Chap. 9, most bioelectric field problems can be formulated in terms of either the Poisson or the Laplace equation for electrical conduction. Since Laplace's equation is the homogeneous counterpart of the Poisson equation, I will develop the treatment for a general three-dimensional Poisson problem and discuss simplifications and special cases when necessary.

A *typical* bioelectric volume conductor can be posed as the following boundary value problem:

$$\nabla \cdot \sigma \nabla \Phi = -I_V \quad \text{in } \Omega \quad (12.1)$$

where  $\Omega$  is the electrostatic potential,  $\sigma$  is the electrical conductivity tensor, and  $I_V$  is the current per unit volume defined within the solution domain,  $\Omega$ . The associated boundary conditions depend on what type of problem one wishes to solve. There are generally considered to be two different types of direct and inverse volume conductor problems.

One type of problem deals with the interplay between the description of the bioelectric volume source currents and the resulting volume currents and volume and surface voltages. Here, the problem statement would be to solve Eq. (12.1) for  $\Phi$  with a known description of  $I_V$  and the Neumann boundary condition:

$$\sigma \nabla \Phi \cdot \mathbf{n} = 0 \quad \text{in } \Gamma_T \quad (12.2)$$

which says that the normal component of the electric field is zero on the surface interfacing with air (here denoted by  $\Gamma_T$ ). This problem can be used to solve two well-known problems in medicine, the direct EEG (electroencephalography) and ECG (electrocardiography) volume conductor problems. In the direct EEG problem, one usually discretizes the brain and surrounding tissue and skull. One then assumes a description of the bioelectric current source within the brain (this usually takes the form of dipoles or multipoles) and calculates the field within the brain and on the surface of the scalp. Similarly, in one version of the direct EEG problem, one utilizes descriptions of the current sources in the heart (either dipoles or membrane current source models such as the FitzHugh-Nagumo and Beeler-Reuter, among others) and calculates the currents and voltages within the volume conductor of the chest and voltages on the surface of the torso. The inverse problems associated with these direct problems involve estimating the current sources  $I_V$  within the volume conductor from measurements of voltages on the surface of either the head or body. Thus one would solve Eq. (12.1) with the boundary conditions

$$\Phi = \Phi_0 \quad \text{on } \Sigma \subseteq \Gamma_T \quad (12.3)$$

$$\sigma \nabla \Phi \cdot \mathbf{n} = 0 \quad \text{on } \Gamma_T \quad (12.4)$$

The first is the Dirichlet condition, which says that one has a set of discrete measurements of the voltage of a subset of the outer surface. The second is the natural Neumann condition. While it does not look much different than the formulation of the direct problem, the inverse formulations are ill-posed. The bioelectric inverse problem in terms of primary current sources does not have a unique solution, and the solution does not depend continuously on the data. Thus, to obtain *useful* solutions, one must try to restrict the solution domain (i.e., number of physiologically plausible solutions) [11] for the former case and apply so-called regularization techniques to attempt to restore the continuity of the solution on the data in the latter case.

Another bioelectric direct/inverse formulation poses both the problems in terms of scalar values at the surfaces. For the EEG problem, one would take the surface of the brain (cortex) as one bounded surface and the surface of the scalp as the other surface. The direct problem would involve making measurements of voltage of the surface of the cortex at discrete locations and then calculating the voltages

on the surface of the scalp. Similarly, for the ECG problem, voltages could be measured on the surface of the heart and used to calculate the voltages at the surface of the torso, as well as within the volume conductor of the thorax. To formulate the inverse problems, one uses measurements on the surface of the scalp (torso) to calculate the voltages on the surface of the cortex (heart). Here, we solve Laplace's equation instead of Poisson's equation, because we are interested in the distributions of voltages on a surface instead of current sources within a volume. This leads to the following boundary value problem:

$$\nabla \cdot \sigma \nabla \Phi = 0 \quad \text{in } \Omega \quad (12.5)$$

$$\Phi = \Phi_0 \quad \text{on } \Sigma \subseteq \Gamma_T \quad (12.6)$$

$$\sigma \nabla \Phi \cdot \mathbf{n} = 0 \quad \text{on } \Gamma_T \quad (12.7)$$

For this formulation, the solution to the inverse problem is unique [17]; however, there still exists the problem of continuity of the solution on the data. The linear algebra counterpart to the elliptic boundary value problem is often useful in discussing this problem of noncontinuity. The numerical solution to all elliptic boundary value problems (such as Poisson and Laplace problems) can be formulated in terms of a set of linear equations  $\mathbf{A}\Phi = \mathbf{b}$ . For the solution of Laplace's equation, the system can be reformulated as

$$\mathbf{A}\Phi_{\text{in}} = \Phi_{\text{out}} \quad (12.8)$$

where  $\Phi_{\text{in}}$  is the vector of data on the inner surface bounding the solution domain (the electrostatic potentials on the cortex or heart, for example),  $\Phi_{\text{out}}$  is the vector of data that bound the outer surface (the subset of voltage values on the surface of the scalp or torso, for example), and  $A$  is the *transfer matrix* between  $\Phi_{\text{out}}$  and  $\Phi_{\text{in}}$ , which usually contains the geometry and physical properties (conductivities, dielectric constants, etc.) of the volume conductor. The direct problem is then simply (well) posed as solving Eq. (12.8) for  $\Phi_{\text{out}}$  given  $\Phi_{\text{in}}$ . Likewise, the inverse problem is to determine  $\Phi_{\text{in}}$  given  $\Phi_{\text{out}}$ .

A characteristic of  $A$  for ill-posed problems is that it has a very large condition number. In other words, the ill-conditioned matrix  $A$  is very near to being singular. Briefly, the condition number is defined as  $\kappa(A) = \|A\| \cdot \|A^{-1}\|$  or the ratio of maximum to minimum singular values measured in the  $L_2$  norm. The ideal problem conditioning occurs for orthogonal matrices which have  $\kappa(A) \approx 1$ , while an ill-conditioned matrix will have  $\kappa(A) \gg 1$ . When one inverts a matrix that has a very large condition number, the inversion process is unstable and is highly susceptible to errors. The condition of a matrix is relative. It is related to the precision level of computations and is a function of the size of the problem. For example, if the condition number exceeds a linear growth rate with respect to the size of the problem, the problem will become increasingly ill-conditioned. See [36] for more about the condition number of matrices.

A number of techniques have arisen to deal with ill-posed inverse problems. These techniques include truncated singular value decomposition (TSVD), generalized singular value decomposition (GSVD), maximum entropy, and a number of generalized least squares schemes, including Twomey and Tikhonov regularization methods. Since this chapter is concerned more with the numerical techniques for approximating bioelectric field problems, the reader is referred to [12–15] to further investigate the regularization of ill-posed problems. A particularly useful reference for discrete ill-posed problems is the Matlab package developed by Per Christian Hansen, which is available via netlib [16].

## 12.2 Model Construction and Mesh Generation

Once we have stated or derived the mathematical equations that define the physics of the system, we must figure out how to solve these equations for the particular domain we are interested in. Most numerical methods for solving boundary value problems require that the continuous domain be broken

up into discrete elements, the so-called mesh or grid, which one can use to approximate the governing equation(s) using the particular numerical technique (finite element, boundary element, finite difference, or multigrid) best suited to the problem.

Because of the complex geometries often associated with bioelectric field problems, construction of the polygonal mesh can become one of the most time-consuming aspects of the modeling process. After deciding on the particular approximation method to use (and the most appropriate type of element), one needs to construct a mesh of the solution domain that matches the number of degrees of freedom of the fundamental element. For the sake of simplicity, we will assume that we will use linear elements, either tetrahedrons, which are usually used for modeling irregular three-dimensional domains, or hexahedrons, which are used for modeling regular, uniform domains.

There are several different strategies for discretizing the geometry into fundamental elements. For bioelectric field problems, two approaches to mesh generation have become standard: the *divide and conquer* (or subsequent subdivision) strategy and the *Delaunay triangulation* strategy.

In using the divide and conquer strategy, one starts with a set of points that define the bounding surface(s) in three dimensions (contours in two dimensions). The volume (surface) is repeatedly divided into smaller regions until a satisfactory discretization level has been achieved. Usually, the domain is broken up into eight-node cubic elements, which can then be subdivided into five (minimally) or six tetrahedral elements if so desired. This methodology has the advantage of being fairly easy to program; furthermore, commercial mesh generators exist for the divide and conquer method. For use in solving bioelectric field problems, its main disadvantage is that it allows elements to overlap interior boundaries. A single element may span two different conductive regions, for example, when part of an element represents muscle tissue (which could be anisotropic) and the other part of the element falls into a region representing fat tissue. It then becomes very difficult to assign unique conductivity parameters to each element and at the same time accurately represent the geometry.

A second method of mesh generation is the Delaunay triangulation strategy. Given a three-dimensional set of points that define the boundaries and interior regions of the domain to be modeled, one tessellates the point cloud into an optimal mesh of tetrahedra. For bioelectric field problems, the advantages and disadvantages tend to be exactly contrary to those arising from the divide and conquer strategy. The primary advantage is that one can create the mesh to fit any predefined geometry, including subsurfaces, by starting with points that define all the necessary surfaces and subsurfaces and then adding additional interior points to minimize the aspect ratio. For tetrahedra, the aspect ratio can be defined as  $4\sqrt{3}/2(\rho_k/h_k)$ , where  $\rho_k$  denotes the diameter of the sphere circumscribed about the tetrahedron, and  $h_k$  is the maximum distance between two vertices. These formulations yield a value of 1 for an equilateral tetrahedron and a value of 0 for a degenerate (flat) element [18]. The closer to the value of 1, the better. The Delaunay criterion is a method for minimizing the occurrence of obtuse angles in the mesh, yielding elements that have aspect ratios as close to 1 as possible, given the available point set. While the ideas behind Delaunay triangulation are straightforward, the programming is nontrivial and is the primary drawback to this method. Fortunately, there exist public domain, two-dimensional versions, including one from netlib called sweep2.c from the directory Voronoi, as well as at least one three-dimensional package [41]. For more information on mesh generation and various aspects of biomedical modeling, see [19–27].

## 12.3 Numerical Methods

---

Because of the geometric complexity of and numerous inhomogeneities inherent in anatomic structures in physiologic models, solutions of bioelectric field problems are usually tractable (except in the most simplified of models) only when one employs a numerical approximation method such as the finite difference (FD), the finite element (FE), boundary element (BE), or the multigrid (MG) method to solve the governing field equation(s).

## Approximation Techniques: The Galerkin Method

The problem posed in Eq. (12.1) can be solved using any of the aforementioned approximation schemes. One technique that addresses three of the previously mentioned techniques (FD, FE, and BE) can be derived by the Galerkin method. The Galerkin method is one of the most widely used methods for discretizing elliptic boundary value problems such as Eq. (12.1) and for treating the spatial portion of time-dependent parabolic problems, which are common in models of cardiac wave propagation. While the Galerkin technique is not essential to the application of any of the techniques, it provides for a unifying bridge between the various numerical methods. To express the problem in a Galerkin form, one begins by rewriting Eq. (12.1) as

$$A\Phi = -I_v \quad (12.9)$$

where  $A$  is the differential operator,  $A = \nabla \cdot (\sigma \nabla)$ . An equivalent statement of Eq. (12.9) is, find  $\Phi$  such that  $(A\Phi + I_v, \bar{\Phi}) = 0$ . Here,  $\bar{\Phi}$  is an arbitrary *test function*, which can be thought of physically as a virtual potential field, and the notation  $(\phi_1, \phi_2) \equiv \int_{\Omega} \phi_1 \phi_2 d\Omega$  denotes the inner products in  $L_2(\Omega)$ . Applying Green's theorem, one can equivalently write

$$(\sigma \nabla \Phi, \nabla \bar{\Phi}) - \left\langle \frac{\partial \Phi}{\partial n}, \bar{\Phi} \right\rangle = -(I_v, \bar{\Phi}) \quad (12.10)$$

where the notation  $\langle \phi_1, \phi_2 \rangle \equiv \int_S \phi_1 \phi_2 dS$  denotes the inner product on the boundary  $S$ . When the Dirichlet,  $\Phi = \Phi_0$ , and Neumann,  $\sigma \nabla \Phi \cdot \mathbf{n} = 0$ , boundary conditions are specified on  $S$ , one obtains the weak form of Eq. (12.1):

$$(\sigma \nabla \Phi, \nabla \bar{\Phi}) = -(I_v, \bar{\Phi}). \quad (12.11)$$

It is understood that this equation must hold for all test functions  $\bar{\Phi}$ , which must vanish at the boundaries where  $\Phi = \Phi_0$ . The Galerkin approximation  $\phi$  to the weak-form solution  $\Phi$  in Eq. (12.11) can be expressed as

$$\phi(x) = \sum_{i=0}^N \phi_i \psi_i(x) \quad (12.12)$$

The trial functions  $\psi_i$ ,  $i = 0, 1, \dots, N$  form a basis for an  $N + 1$  dimensional space  $S$ . One can define the *Galerkin approximation* to be the element  $\phi \in S$  that satisfies

$$(\sigma \nabla \phi, \nabla \psi_j) = -(I_v, \psi_j) \quad (\forall \psi_j \in S) \quad (12.13)$$

Since our differential operator  $A$  is positive definite and self adjoint [i.e.,  $(A\Phi, \Phi) \geq \alpha(\Phi, \Phi) > 0$  for some nonzero positive constant  $\alpha$  and  $(A\Phi, \bar{\Phi}) = (\Phi, A\bar{\Phi})$ , respectively], then we can define a space  $E$  with an inner product defined as  $(\Phi, \bar{\Phi})_E = (A\Phi, \bar{\Phi}) \equiv a(\Phi, \bar{\Phi})$  and norm (the so-called energy norm) equal to

$$\|\Phi\|_E = \left\{ \int_{\Omega} (\nabla \Phi)^2 d\Omega \right\}^{\frac{1}{2}} = (\Phi, \Phi)_E^{\frac{1}{2}} \quad (12.14)$$

The solution  $\Phi$  of Eq. (12.9) satisfies

$$(A\Phi, \psi_i) = -(I_v, \psi_i) \quad (\forall \psi_i \in S) \quad (12.15)$$

and the approximate Galerkin solution obtained by solving Eq. (12.13) satisfies

$$(A\phi, \psi_i) = -(I_v, \psi_i) \quad (\forall \psi_i \in S) \quad (12.16)$$

Subtracting Eq. (12.15) from Eq. (12.16) yields

$$(A(\phi - \Phi), \psi_i) = (\phi - \bar{\phi}, \psi_i)_E = 0 \quad (\forall \psi_i \in S) \quad (12.17)$$

The difference  $\phi - \Phi$  denotes the error between the solution in the finite dimensional space  $V$  and the  $N + 1$  dimensional space  $S$ . Equation (12.17) states that the error is orthogonal to all basis functions spanning the space of possible Galerkin solutions. Consequently, the error is orthogonal to all elements in  $S$  and must therefore be the minimum error. Thus the Galerkin approximation is an orthogonal projection of the true solution  $\Phi$  onto the given finite dimensional space of possible approximate solutions. Therefore, the Galerkin approximation is the best approximation in the energy space  $E$ . Since the operator is positive definite, the approximate solution is unique. Assume for a moment that there are two solutions,  $\phi_1$  and  $\phi_2$ , satisfying

$$(A\phi_1, \psi_i) = -(I_v, \psi_i) \quad (A\phi_2, \psi_i) = -(I_v, \psi_i) \quad (\forall \psi_i \in S) \quad (12.18)$$

respectively. Then the difference yields

$$(A(\phi_1 - \phi_2), \psi_i) = 0 \quad (\forall \psi_i \in S) \quad (12.19)$$

The function arising from subtracting one member from another member in  $S$  also belongs in  $S$ ; hence the difference function can be expressed by the set of  $A$  orthogonal basis functions spanning  $S$ :

$$\sum_{j=0}^N \Delta\phi_j (A(\psi_j, \psi_i)) = 0 \quad (\forall \psi_i \in S) \quad (12.20)$$

When  $i \neq j$ , the terms vanish due to the basis functions being orthogonal with respect to  $A$ . Since  $A$  is positive definite,

$$(A\Phi_i, \Phi_i) > 0 \quad i = 0, \dots, N \quad (12.21)$$

Thus  $\Delta\phi_i = 0, i = 0, \dots, N$ , and by virtue of Eq. (12.20),  $\delta\phi = 0$ , such that  $\phi_1 = \phi_2$ . The identity contradicts the assumption of two distinct Galerkin solutions. This proves the solution is unique [28].

## The Finite-Difference Method

Perhaps the most traditional way to solve Eq. (12.1) utilizes the finite-difference approach by discretizing the solution domain  $\Omega$  using a grid of uniform hexahedral elements. The coordinates of a typical grid

point are  $x = lh$ ,  $y = mh$ ,  $z = nh$  ( $l, m, n = \text{integers}$ ), and the value of  $\Phi(x, y, z)$  at a grid point is denoted by  $\Phi_{l,m,n}$ . Taylor's theorem can then be used to provide the difference equations. For example,

$$\Phi_{l+1,m,n} = \left( \Phi + h \frac{\partial \Phi}{\partial x} + \frac{1}{2} h^2 \frac{\partial^2 \Phi}{\partial x^2} + \frac{1}{6} h^3 \frac{\partial^3 \Phi}{\partial x^3} + \dots \right)_{l,m,n} \quad (12.22)$$

with similar equations for  $\Phi_{l-1,m,n}$ ,  $\Phi_{l,m+1,n}$ ,  $\Phi_{l,m-1,n}$ , ... The finite-difference representation of Eq. (12.1) is

$$\begin{aligned} & \frac{\Phi_{l+1,m,n} - 2\Phi_{l,m,n} + \Phi_{l-1,m,n}}{h^2} + \frac{\Phi_{l,m+1,n} - 2\Phi_{l,m,n} + \Phi_{l,m-1,n}}{h^2} \\ & + \frac{\Phi_{l,m,n+1} - 2\Phi_{l,m,n} + \Phi_{l,m,n-1}}{h^2} = -I_{l,m,n}(v) \end{aligned} \quad (12.23)$$

or, equivalently,

$$\Phi_{l+1,m,n} + \Phi_{l-1,m,n} + \Phi_{l,m+1,n} + \Phi_{l,m-1,n} + \Phi_{l,m,n+1} + \Phi_{l,m,n-1} - 6\Phi_{l,m,n} = -h^2 I_{l,m,n}(v) \quad (12.24)$$

If one defines the vector  $\Phi$  to be  $[\Phi_{1,1,1} \dots \Phi_{1,1,N-1} \dots \Phi_{1,N-1,1} \dots \Phi_{N-1,N-1,N-1}]^T$  to designate the  $(N-1)^3$  unknown grid values and pull out all the known information from (24), one can reformulate Eq. (12.1) by its finite-difference approximation in the form of the matrix equation  $A\Phi = \mathbf{b}$ , where  $\mathbf{b}$  is a vector that contains the sources and modifications due to the Dirichlet boundary condition.

Unlike the traditional Taylor's series expansion method, the Galerkin approach utilizes basis functions, such as linear piecewise polynomials, to approximate the true solution. For example, the Galerkin approximation to sample problem (12.1) would require evaluating Eq. (12.13) for the specific grid formation and specific choice of basis function:

$$\int_{\Omega} \left( \sigma_x \frac{\partial \phi}{\partial x} \frac{\partial \psi_i}{\partial x} + \sigma_y \frac{\partial \phi}{\partial y} \frac{\partial \psi_i}{\partial y} + \sigma_z \frac{\partial \phi}{\partial z} \frac{\partial \psi_i}{\partial z} \right) d\Omega = - \int_{\Omega} I_v \psi_i d\Omega \quad (12.25)$$

Difference quotients are then used to approximate the derivatives in Eq. (12.25). Note that if linear basis functions are utilized in Eq. (12.25), one obtains a formulation that corresponds exactly with the standard finite-difference operator. Regardless of the difference scheme or order of basis function, the approximation results in a linear system of equations of the form  $A\Phi = \mathbf{b}$ , subject to the appropriate boundary conditions.

## The Finite-Element Method

As seen earlier, in the classic numerical treatment for partial differential equation—the finite-difference method—the solution domain is approximated by a grid of uniformly spaced nodes. At each node, the governing differential equation is approximated by an algebraic expression that references adjacent grid points. A system of equations is obtained by evaluating the previous algebraic approximations for each node in the domain. Finally, the system is solved for each value of the dependent variable at each node. In the finite-element method, the solution domain can be discretized into a number of uniform or nonuniform finite elements that are connected via nodes. The change of the dependent variable with regard to location is approximated within each element by an interpolation function. The interpolation function is defined relative to the values of the variable at the nodes associated with each element. The original boundary value problem is then replaced with an equivalent integral formulation [such as

Eq. (12.13)]. The interpolation functions are then substituted into the integral equation, integrated, and combined with the results from all other elements in the solution domain. The results of this procedure can be reformulated into a matrix equation of the form  $A\Phi = \mathbf{b}$ , which is subsequently solved for the unknown variables [20, 29].

The formulation of the finite-element approximation starts with the Galerkin approximation,  $(\sigma \nabla \Phi, \nabla \bar{\Phi}) = -(I_v, \bar{\Phi})$ , where  $\bar{\Phi}$  is our test function. Now one can use the finite-element method to turn the continuous problems into a discrete formulation. First, one discretizes the solution domain,  $\Omega = \bigcup_{e=1}^E \Omega_e$  and defines a finite dimensional subspace  $V_h \subset V = \{\bar{\Phi}: \bar{\Phi} \text{ is continuous on } \Omega, \nabla \bar{\Phi} \text{ is piecewise continuous on } \Omega\}$ . One usually defines parameters of the function  $\bar{\Phi} \in V_h$  at node points  $\alpha_i = \bar{\Phi}(x_i)$ ,  $i = 0, 1, \dots, N$ . If one now defines the basis functions  $\psi_i \in V_h$  as linear continuous piecewise functions that take the value 1 at node points and zero at other node points, then one can represent the function  $\bar{\Phi} \in V_h$  as

$$\bar{\Phi}(x) = \sum_{i=0}^N d_i \psi_i(x) \quad (12.26)$$

such that each  $\bar{\Phi} \in V_h$  can be written in a unique way as a linear combination of the basis functions  $\psi_i \in V_h$ . Now the finite-element approximation of the original boundary value problem can be stated as

$$\text{Find } \Phi_h \in V_h \text{ such that } (\sigma \nabla \Phi_h, \nabla \bar{\Phi}) = -(I_v, \bar{\Phi}) \quad (12.27)$$

Furthermore, if  $\Phi_h \in V_h$  satisfies problem (12.27), then we have  $(\sigma \nabla \Phi_h, \nabla \Psi_i) = -(I_v, \Psi_i)$  [30]. Finally, since  $\Phi_h$  itself can be expressed as the linear combination

$$\Phi_h = \sum_{i=0}^N \xi_i \Psi_i(x) \quad \xi_i = \Phi_h(x_i) \quad (12.28)$$

one can then write problem (12.27) as

$$\sum_{i=0}^N \xi_i (\sigma_{ij} \nabla \Psi_i, \nabla \Psi_j) = -(I_v, \Psi_j) \quad j=0, \dots, N \quad (12.29)$$

subject to the Dirichlet boundary condition. Then the finite-element approximation of Eq. (12.1) can equivalently be expressed as a system of  $N$  equations with  $N$  unknowns  $\xi_0, \dots, \xi_N$  (the electrostatic potentials, for example). In matrix form, the preceding system can be written as  $A\xi = b$ , where  $A = (a_{ij})$  is called the *global stiffness matrix* and has elements  $(a_{ij}) = (\sigma_{ij} \nabla \Psi_i, \nabla \Psi_j)$ , while  $b_i = -(I_v, \Psi_i)$  and is usually termed the *load vector*.

For volume conductor problems,  $A$  contains all the geometry and conductivity information of the model. The matrix  $A$  is symmetric and positive definite; thus it is nonsingular and has a unique solution. Because the basis function differs from zero for only a few intervals,  $A$  is sparse (only a few of its entries are nonzero).

### Application of the FE Method for 3D Domains

Now let us illustrate the concepts of the finite-element method by considering the solution of Eq. (12.1) using linear three-dimensional elements. One starts with a 3D domain  $\Omega$  that represents the geometry of our volume conductor and breaks it up into discrete elements to form a finite dimensional subspace  $\Omega_h$ . For 3D domains, one has the choice of representing the function as either tetrahedra

$$\tilde{\Phi} = \alpha_1 + \alpha_2 x + \alpha_3 y + \alpha_4 z, \quad (12.30)$$

or hexahedra

$$\tilde{\Phi} = \alpha_1 + \alpha_2 x + \alpha_3 y + \alpha_4 z + \alpha_5 xy + \alpha_6 yz + \alpha_7 xz + \alpha_8 xyz \quad (12.31)$$

Because of space limitations, let us restrict the development to tetrahedra, knowing that it is easy to modify the formulas for hexahedra. Take out a specific tetrahedra from the finite dimensional subspace and apply the previous formulations for the four vertices:

$$\begin{pmatrix} \tilde{\Phi}_1 \\ \tilde{\Phi}_2 \\ \tilde{\Phi}_3 \\ \tilde{\Phi}_4 \end{pmatrix} = \begin{pmatrix} 1 & x_1 & y_1 & z_1 \\ 1 & x_2 & y_2 & z_2 \\ 1 & x_3 & y_3 & z_3 \\ 1 & x_4 & y_4 & z_4 \end{pmatrix} \begin{pmatrix} \alpha_1 \\ \alpha_2 \\ \alpha_3 \\ \alpha_4 \end{pmatrix} \quad (12.32)$$

or

$$\tilde{\Phi}_i = \mathbf{C}\alpha \quad (12.33)$$

which define the coordinate vertices, and

$$\alpha = \mathbf{C}^{-1}\tilde{\Phi}_i \quad (12.34)$$

which defines the coefficients. From Eqs. (12.30) and (12.34) one can express  $\tilde{\Phi}$  at any point within the tetrahedra,

$$\tilde{\Phi} = [1, x, y, z]\alpha = \mathbf{S}\alpha = \mathbf{S}\mathbf{C}^{-1}\tilde{\Phi}_i \quad (12.35)$$

or, most succinctly,

$$\tilde{\Phi} = \sum_i N_i \tilde{\Phi}_i \quad (12.36)$$

$\tilde{\Phi}_i$  is the solution value at node  $i$ , and  $\mathbf{N} = \mathbf{S}\mathbf{C}^{-1}$  is the local *shape function* or *basis function*. This can be expressed in a variety of ways in the literature (depending, usually, on whether you are reading engineering or mathematical treatments of finite element analysis):

$$\Phi_j(N_i) = N_i(x, y, z) = f_i(x, y, z) \equiv \frac{a_i + b_i x + c_i y + d_i z}{6V} \quad (12.37)$$

where

$$6V = \begin{vmatrix} 1 & x_1 & y_1 & z_1 \\ 1 & x_2 & y_2 & z_2 \\ 1 & x_3 & y_3 & z_3 \\ 1 & x_4 & y_4 & z_4 \end{vmatrix} \quad (12.38)$$

defines the volume of the tetrahedra  $V$ .

Now that a suitable set of basis functions is available, one can find the finite-element approximation to the 3D problem. The original problem can be formulated as

$$a(u, v) = (I_v, v) \quad \forall v \in \Omega \quad (12.39)$$

where

$$a(u, v) = \int_{\Omega} \nabla u \cdot \nabla v d\Omega \quad (12.40)$$

and

$$(I_v, v) = \int_{\Omega} I_v \cdot v d\Omega \quad (12.41)$$

The finite-element approximation to the original boundary value problem is

$$a(u_h, v) = (I_v, v) \quad \forall v \in \Omega_h \quad (12.42)$$

which has the equivalent form

$$\sum_{i=1}^N \xi_i a(\Phi_i, \Phi_j) = (I_v, \Phi_j) \quad (12.43)$$

where

$$a(\Phi_i, \Phi_j) = a(\Phi_i, (N_j), \Phi_j (N_i)) \quad (12.44)$$

which can be expressed by the matrix and vector elements.

$$(a_{ij}) = \int_{\Omega_E} \left( \frac{\partial N_i}{\partial x} \frac{\partial N_j}{\partial x} + \frac{\partial N_i}{\partial y} \frac{\partial N_j}{\partial y} + \frac{\partial N_i}{\partial z} \frac{\partial N_j}{\partial z} \right) d\Omega \quad (12.45)$$

and

$$I_i = \int_{\Omega_E} N_i I_v d\Omega \quad (12.46)$$

Fortunately, these quantities are easy to evaluate for linear tetrahedra. As a matter of fact, there are closed-form solutions for the matrix elements  $(a_{ij})$ :

$$\int_{\Omega_h} N_1^a N_2^b N_3^c N_4^d d\Omega = 6V \frac{a!b!c!d!}{(a+b+c+d+3)!} \quad (12.47)$$

Therefore,

$$(a_{ij}) = \int_{\Omega_E} \frac{b_i b_j + c_i c_j + d_i d_j}{6V^2} d\Omega = \frac{b_i b_j + c_i c_j + d_i d_j}{6V} \quad (12.48)$$

and, for the right hand side, one has, assuming constant sources,

$$I_i = \int \frac{a_i + b_i x + c_i y + d_i z}{6V} I_v d\Omega = \frac{VI_v}{4} \quad (12.49)$$

which have the compact forms

$$a_{ij}^{(n)} = \frac{1}{6V} \left( b_i^{(n)} b_j^{(n)} + c_i^{(n)} c_j^{(n)} + d_i^{(n)} + d_j^{(n)} \right) \quad (12.50)$$

and

$$I_i^{(n)} = \frac{VI_v}{4} \quad \text{for constant sources} \quad (12.51)$$

Now one adds up all the contributions from each element into a global matrix and global vector:

$$\sum_{n=1}^{N_{el}} \left( a_{ij}^{(n)} \right) \left( \xi_i \right) = \left( I_i^{(n)} \right) \quad (12.52)$$

where  $N_{el}$  is equal to the total number of elements in the discretized solution domain, and  $i$  represents the node numbers (vertices). This yields a linear system of equations of the form  $\mathbf{A}\Phi = \mathbf{b}$ , where  $\Phi$  is the solution vector of voltages,  $\mathbf{A}$  represents the geometry and conductivity of the volume conductor, and  $\mathbf{b}$  represents the contributions from the current sources and boundary conditions.

For the finite-difference method, it turns out that the Dirichlet boundary condition is easy to apply, while the Neumann condition takes a little extra effort. For the finite-element method, it is just the opposite. The Neumann boundary condition

$$\nabla\Phi \cdot \mathbf{n} = 0 \quad (12.53)$$

is satisfied automatically within the Galerkin and variational formulations. This can be seen by using Green's divergence theorem,

$$\int_{\Omega} \nabla \cdot \mathbf{A} dx = \int_{\Gamma} \mathbf{A} \cdot \mathbf{n} dS \quad (12.54)$$

and applying it to the left-hand side of the Galerkin finite-element formulation:

$$\begin{aligned} \int_{\Omega} \nabla v \cdot \nabla w d\Omega &\equiv \int_{\Omega} \left( \frac{\partial v}{\partial x_1} \frac{\partial w}{\partial x_1} + \frac{\partial v}{\partial x_2} \frac{\partial w}{\partial x_2} \right) d\Omega \\ &= \int_{\Gamma} \left( v \frac{\partial w}{\partial x_1} n_1 + v \frac{\partial w}{\partial x_2} n_2 \right) dS - \int_{\Omega} v \left( \frac{\partial^2 w}{\partial x_1^2} + \frac{\partial^2 w}{\partial x_2^2} n_2 \right) d\Omega \\ &= \int_{\Gamma} v \frac{\partial w}{\partial n} dS - \int_{\Omega} v \nabla^2 w d\Omega \end{aligned} \quad (12.55)$$

If one multiplies the original differential equation,  $\nabla^2\Phi = -I_v$ , by an arbitrary test function and integrates, one obtains

$$\left(I_v, v\right) = -\int_{\Omega} \left(\nabla^2\Phi\right)_v d\Omega = -\int_{\Gamma} \frac{\partial\Phi}{\partial n} v dS + \int_{\Omega} \nabla\Phi \cdot \nabla v d\Omega = a\left(\Phi, v\right) \quad (12.56)$$

where the boundary integral term  $\partial\Phi/\partial n$  vanishes, and one obtains the standard Galerkin finite-element formulation.

To apply the Dirichlet condition, one has to work a bit harder. To apply the Dirichlet boundary condition directly, one usually modifies the  $(a_{ij})$  matrix and  $b_i$  vector such that one can use standard linear system solvers. This is accomplished by implementing the following steps. Assuming that the  $i$ th value of  $u_i$  is known,

1. Subtract from the  $i$ th member of the right-hand side the product of  $a_{ij}$  and the known value of  $\Phi_i$  (call it  $\bar{\Phi}_i$ ); this yields the new right-hand side,  $\hat{b}_i = b_i - a_{ij}\bar{\Phi}_i$ .
2. Zero the  $i$ th row and column of  $A$ :  $\hat{a}_{ij} = \hat{a}_{ji} = 0$ .
3. Assign  $\hat{a}_{ii} = 1$ .
4. Set the  $j$ th member of the right-hand side equal to  $\Phi_i$ .
5. Continue for each Dirichlet condition.
6. Solve the augmented system  $\hat{A}\hat{\Phi} = \hat{b}_v$ .

## The Boundary-Element Method

The bioelectric field problems with isotropic domains (and few inhomogeneities), another technique, called the *boundary-element method*, may be used. This technique utilizes information only on the boundaries of interest and thus reduces the dimension of any field problem by one. For differential operators, the response at any given point to sources and boundary conditions depends only on the response at neighboring points. The FD and FE methods approximate differential operators defined on subregions (volume elements) in the domain; hence direct mutual influence (connectivity) exists only between neighboring elements, and the coefficient matrices generated by these methods have relatively few nonzero coefficients in any given matrix row. As is demonstrated by Maxwell's laws, equations in differential forms often can be replaced by equations in integral forms; e.g., the potential distribution in a domain is uniquely defined by the volume sources and the potential and current density on the boundary. The boundary-element method uses this fact by transforming the differential operators defined in the domain to integral operators defined on the boundary. In the boundary-element method [31–33], only the boundary is discretized; hence the mesh generation is considerably simpler for this method than for the volume methods. Boundary solutions are obtained directly by solving the set of linear equations; however, potentials and gradients in the domain can be evaluated only after the boundary solutions have been obtained. Since this method has a rich history in bioelectric field problems, the reader is referred to some of the classic references for further information regarding the application of the BE method to bioelectric field problems [6, 42–44].

## Solution Methods and Computational Considerations

Application of each of the previous approximation methods to Eq. (12.1) yields a system of linear equations of the form  $\mathbf{A}\Phi = \mathbf{b}$ , which must be solved to obtain the final solution. There is a plethora of available techniques for the solutions of such systems. The solution techniques can be broadly categorized as *direct* and *iterative* solvers. Direct solvers include Gaussian elimination and LU decomposition, while iterative methods include Jacobi, Gauss-Seidel, successive overrelaxation (SOR), and conjugate gradient (CG) methods, among others. The choice of the particular solution method is highly dependent on the approximation technique employed to obtain the linear system, on the size of the resulting system, and

on accessible computational resources. For example, the linear system resulting from the application of the FD or FE method will yield a matrix  $\mathbf{A}$  that is symmetric, positive definite, and sparse. The matrix resulting from the FD method will have a specific band-diagonal structure that is dependent on the order of difference equations one uses to approximate the governing equation. The matrix resulting from the FE method will be exceedingly sparse and only a few of the off-diagonal elements will be nonzero. The application of the BE method, on the other hand, will yield a matrix  $\mathbf{A}$  that is dense and nonsymmetric and thus requires a different choice of solver.

The choice of the optimal solver is further complicated by the size of the system versus access to computational resources. Sequential direct methods are usually confined to single workstations, and thus the size of the system should fit in memory for optimal performance. Sequential iterative methods can be employed when the size of the system exceeds the memory of the machine; however, one pays a price in terms of performance, since direct methods are usually much faster than iterative methods. In many cases, the size of the system exceeds the computational capability of a single workstation, and one must resort to the use of clusters of workstations and/or parallel computers.

While new and improved methods continue to appear in the numerical analysis literature, my studies comparing various solution techniques for direct and inverse bioelectric field problems have resulted in the conclusion that the preconditioned conjugate gradient methods and multigrid methods are the best overall performers for volume conductor problems computed on single workstations. Specifically, the incomplete Choleski conjugate gradient (ICCG) method works well for the FE method,<sup>1</sup> and the preconditioned biconjugate gradient (BCG) methods are often used for BE methods. When clusters of workstations and/or parallel architectures are considered, the choice is less clear. For use with some high-performance architectures that contain large amounts of memory, parallel direct methods such as LU decomposition become attractive; however, preconditioned conjugate gradient methods still perform well.

A discussion of parallel computing methods for the solution of biomedical field problems could fill an entire text. Thus the reader is directed to the following references on parallel scientific computing [45–47].

## Comparison of Methods

Since there is not enough space to give a detailed, quantitative description of each of the previously mentioned methods, an abbreviated summary is given of the applicability of each method in solving different types of bioelectric field problems.

As outlined earlier, the FD, FE, and BE methods can all be used to approximate the boundary value problems that arise in biomedical research problems. The choice depends on the nature of the problem. The FE and FD methods are similar in that the entire solution domain must be discretized, while with the BE method only the bounding surfaces must be discretized. For regular domains, the FD method is generally the easiest method to code and implement, but the FD method usually requires special modifications to define irregular boundaries, abrupt changes in material properties, and complex boundary conditions. While typically more difficult to implement, the BE and FE methods are preferred for problems with irregular, inhomogeneous domains and mixed boundary conditions. The FE method is superior to the BE method for representing nonlinearity and true anisotropy, while the BE method is superior to the FE method for problems where only the boundary solution is of interest or where solutions are wanted in a set of highly irregularly spaced points in the domain. Because the computational mesh is simpler for the BE method than for the FE method, the BE program requires less bookkeeping than an FE program. For this reason, BE programs are often considered easier to develop than FE programs; however, the difficulties associated with singular integrals in the BE method are often highly underestimated. In general, the FE method is preferred for problems where the domain is highly heterogeneous, whereas the BE method is preferred for highly homogeneous domains.

---

<sup>1</sup>This is specifically for the FE method applied to elliptic problems. Such problems yield a matrix that is symmetric and positive definite. The Choleski decomposition only exists for symmetric, positive-definite matrices.

## 12.4 Adaptive Methods

Thus far how one formulates the problem, discretizes the geometry, and finds an approximate solution have been discussed. Now one is faced with answering the difficult question pertaining to the accuracy of the solution. Without reference to experimental data, how can one judge the validity of the solutions? To give oneself an intuitive feel for the problem (and possible solution), consider the approximation of a two-dimensional region discretized into triangular elements. The finite-element method will be applied to solve Laplace's equation in the region.

First, consider the approximation of the potential field  $\Phi(x, y)$  by a two-dimensional Taylor's series expansion about a point  $(x, y)$ :

$$\begin{aligned} \Phi(x+h, y+k) = \Phi(x, y) &+ \left[ h \frac{\partial \Phi(x, y)}{\partial x} + k \frac{\partial \Phi(x, y)}{\partial y} \right] \\ &+ \frac{1}{2!} \left[ h^2 \frac{\partial^2 \Phi(x, y)}{\partial^2 x} + 2hk \frac{\partial^2 \Phi(x, y)}{\partial x \partial y} + k^2 \frac{\partial^2 \Phi(x, y)}{\partial^2 y} \right] + \dots \end{aligned} \quad (12.57)$$

where  $h$  and  $k$  are the maximum  $x$  and  $y$  distances within an element. Using the first two terms (up to first-order terms) in the preceding Taylor's expansion, one can obtain the standard linear interpolation function for a triangle:

$$\frac{\partial \Phi(x_i, y_i)}{\partial x} = \frac{1}{2A} \left[ \Phi_i(y_j - y_m) + \Phi_m(y_i - y_j) + \Phi_j(y_m - y_i) \right] \quad (12.58)$$

where  $A$  is the area of the triangle. Likewise, one could calculate the interpolant for the other two nodes and discover that

$$\frac{\partial \Phi(x_i, y_i)}{\partial x} = \frac{\partial \Phi(x_j, y_j)}{\partial x} = \frac{\partial \Phi(x_m, y_m)}{\partial x} \quad (12.59)$$

is constant over the triangle (and thus so is the gradient in  $y$  as well). Thus one can derive the standard linear interpolation formulas on a triangle that represents the first two terms of the Taylor's series expansion. This means that the error due to discretization (from using linear elements) is proportional to the third term of the Taylor's expansion:

$$\epsilon \approx \frac{1}{2!} \left[ h^2 \frac{\partial^2 \Phi(x, y)}{\partial^2 x} + 2hk \frac{\partial^2 \Phi(x, y)}{\partial x \partial y} + k^2 \frac{\partial^2 \Phi(x, y)}{\partial^2 y} \right] \quad (12.60)$$

where  $\Phi$  is the exact solution. One can conjecture, then, that the error due to discretization for first-order linear elements is proportional to the second derivative. If  $\Phi$  is a linear function over the element, then the first derivative is a constant and the second derivative is zero, and there is no error due to discretization. This implies that the gradient must be constant over each element. If the function is not linear or the gradient is not constant over an element, the second derivative will not be zero and is proportional to the error incurred due to "improper" discretization. Examining Eq. (12.60), one can easily see that one way to decrease the error is to decrease the size of  $h$  and  $k$ . As  $h$  and  $k$  go to zero, the error tends to zero as well. Thus decreasing the mesh size in places of high errors due to high gradients decreases the error. As an aside, note that if one divided Eq. (12.9) by  $hk$ , one can also express the error

in terms of the elemental aspect ratio  $h/k$ , which is a measure of the relative shape of the element. It is easy to see that one must be careful to maintain an aspect ratio as close to unity as possible.

The problem with the preceding heuristic argument is that one has to know the exact solution a priori before one can estimate the error. This is certainly a drawback considering that one is trying to accurately approximate  $\Phi$ .

## Convergence of a Sequence of Approximate Solutions

Let's try to quantify the error a bit further. When one considers the preceding example, it seems to make sense that if one increases the number of degrees of freedom used to approximate the function, the accuracy must approach the true solution. That is, one would hope that the sequence of approximate solutions will *converge* to the exact solution as the number of degrees of freedom (DOF) increases indefinitely:

$$\|\Phi(x) - \tilde{\Phi}_n(x)\| \rightarrow 0 \quad \text{as } n \rightarrow \infty \quad (12.61)$$

This is a statement of *pointwise convergence*. It describes the approximate solution as approaching arbitrarily close to the exact solution at each point in the domain as the number of DOF increases.

Measures of convergence often depend on how the *closeness* of measuring the distance between functions is defined. Another common description of measuring convergence is *uniform convergence*, which requires that the maximum value of  $\|\Phi(x) - \tilde{\Phi}_n(x)\|$  in the domain vanish as  $N \rightarrow \infty$ . This is stronger than pointwise convergence because it requires a uniform rate of convergence at every point in the domain. Two other commonly used measures are *convergence in energy* and *convergence in mean*, which involve measuring an *average* of a function of the pointwise error over the domain [40].

In general, proving pointwise convergence is very difficult except in the simplest cases, while proving the convergence of an averaged value, such as energy, is often easier. Of course, scientists and engineers are often much more interested in ensuring that their answers are accurate in a pointwise sense than in an energy sense because they typically want to know values of the solution  $\Phi(x)$  and gradients  $\nabla\Phi(x)$  at specific places.

One intermediate form of convergence is called the *Cauchy convergence*. Here, one requires the sequences of two different approximate solutions to approach arbitrarily close to each other:

$$\|\Phi_m(x) - \tilde{\Phi}_n(x)\| \rightarrow 0 \quad \text{as } m, n \rightarrow \infty \quad (12.62)$$

While the pointwise convergence expression would imply the preceding equation, it is important to note that the Cauchy convergence does not imply pointwise convergence, since the functions could converge to an answer other than the true solution.

While one cannot be assured of pointwise convergence of these functions for all but the simplest cases, there do exist theorems that ensure that a sequence of approximate solutions must converge to the exact solution (assuming no computational errors) if the basis functions satisfy certain conditions. The theorems can only ensure convergence in an average sense over the entire domain, but it is usually the case that if the solution converges in an average sense (energy, etc.), then it will converge in the pointwise sense as well.

## Energy Norms

The error in energy, measured by the *energy norm*, is defined in general as [37–39]

$$\|e\| = \left( \int_{\Omega} e^T L e \, d\Omega \right)^{\frac{1}{2}} \quad (12.63)$$

where  $e = \Phi(x) - \tilde{\Phi}_n(x)$ , and  $L$  is the differential operator for the governing differential equation [i.e., it contains the derivatives operating on  $\Phi(x)$  and any function multiplying  $\Phi(x)$ ]. For physical problems, this is often associated with the energy density.

Another common measure of convergence utilizes the  $L_2$  norm. This can be termed the *average error* and can be associated with errors in any quantity. The  $L_2$  norm is defined as

$$\|e\|_{L_2} = \left( \int_{\Omega} e^T e \, d\Omega \right)^{\frac{1}{2}} \quad (12.64)$$

While the norms given above are defined on the whole domain, one can note that the square of each can be obtained by summing element contributions:

$$\|e\|^2 = \sum_{i=1}^M \|e\|_i^2 \quad (12.65)$$

where  $i$  represents an element contribution and  $m$  the total element number. Often for an *optimal* finite-element mesh, one tries to make the contributions to this square of the norm equal for all elements.

While the absolute values given by the energy or  $L_2$  norms have little value, one can construct a relative percentage error that can be more readily interpreted:

$$\eta = \frac{\|e\|}{\|\Phi\|} \times 100 \quad (12.66)$$

This quantity, in effect, represents a weighted RMS error. The analysis can be determined for the whole domain or for element subdomains. One can use it in an adaptive algorithm by checking element errors against some predefined tolerance  $\eta_0$  and increasing the DOF only of those areas above the predefined tolerance.

Two other methods, the  $p$  and the  $hp$  methods, have been found, in most cases, to converge faster than the  $h$  method. The  $p$  method of refinement requires that one increase the order of the basis function that was used to represent the interpolation (i.e., linear to quadratic to cubic, etc.) The  $hp$  method is a combination of the  $h$  and  $p$  methods and has recently been shown to converge the fastest of the three methods (but, as you might imagine, it is the hardest to implement). To find out more about adaptive refinement methods, see [27, 30, 34, 35, 37, 40].

## Acknowledgments

This work was supported in part by awards from the Whitaker Foundation, the NIH, and the NSF. I would like to thank K. Coles, J. Schmidt, and D. Weinstein for their helpful comments and suggestions. An expanded, educational case studies version of this chapter entitled, “Direct and Inverse Bioelectric Field Problems,” may be found as part of the DOE-sponsored Computational Science Education Program (CSEP). The chapter is available freely via Mosaic at <http://csep1.phy.ornl.gov/csep.html> and contains exercises, projects, and C and Fortran computer codes.

## References

1. Miller CE, Henriquez CS. Finite element analysis of bioelectric phenomena. *Crit Rev Biomed Eng* 18:181, 1990. *This represents the first review paper on the use of the finite-element method as applied to biomedical problems. As the authors note, bioengineers came to these methods only fairly recently as compared with other engineers. It contains a good survey of applications.*
2. Nenonen J, Rajala HM, Katilia T. Biomagnetic Localization and 3D Modelling. Report TKK-F-A689. Espoo, Finland, Helsinki University of Technology, 1992.
3. Johnson CR, MacLeod RS, Ershler PR. A computer model for the study of electrical current flow in the human thorax. *Comput Biol Med* 22(3):305, 1992. *This paper details the construction of a three-dimensional thorax model.*
4. Johnson CR, MacLeod RS, Matheson MA. Computer simulations reveal complexity of electrical activity in the human thorax. *Comput Phys* 6(3):230, 1992. *This paper deals with the computational and visualization aspects of the forward ECG problem.*
5. Kim Y, Fahy JB, Tupper BJ. Optimal electrode designs for electrosurgery. *IEEE Trans Biomed Eng* 33:845, 1986. *This paper discusses an example of the modeling of bioelectric fields for applications in surgery.*
6. Plonsey R. *Bioelectric Phenomena*. New York, McGraw-Hill, 1969. *This is the first text using physics, mathematics, and engineering principles to quantify bioelectric phenomena.*
7. Henriquez CS, Plonsey R. Simulation of propagation along a bundle of cardiac tissue. I. Mathematical formulation. *IEEE Trans Biomed Eng* 37:850, 1990. *This paper and the companion paper below describe the bidomain approach to the propagation of electrical signals through active cardiac tissue.*
8. Henriquez CS, Plonsey R. Simulation of propagation along a bundle of cardiac tissue: II. Results of simulation. *IEEE Trans Biomed Eng* 37:861, 1990.
9. Keener JP. Waves in excitable media. *SIAM J Appl Math* 46:1039, 1980. *This paper describes mathematical models for wave propagation in various excitable media. Both chemical and physiologic systems are addressed.*
10. Hadamard J. Sur les problemes aux derivees parielies et leur signification physique. *Bull Univ Princeton*, pp 49–52, 1902. *This is Hadamard's original paper describing the concepts of well- and ill-posedness, in French.*
11. Greensite F, Huiskamp G, van Oosterom A. New quantitative and qualitative approaches to the inverse problem of electrocardiography: Their theoretical relationship and experimental consistency. *Med Phy* 17(3):369, 1990. *This paper describes methods for constraining the inverse problem of electrocardiology in terms of sources. Methods are developed which put bounds on the space of acceptable solutions.*
12. Tikhonov A, Arsenin V. *Solution of Ill-Posed Problems*. Washington, Winston, 1977. *This is the book in which Tikhonov describes his method of regularization for ill-posed problems.*
13. Tikhonov AN, Goncharsky AV. *Ill-Posed Problems in the Natural Sciences*. Moscow, MIR Publishers, 1987. *This is a collection of research papers from physics, geophysics, optics, medicine, etc., which describe ill-posed problems and the solution techniques the authors have developed.*
14. Glasko VB. *Inverse Problems of Mathematical Physics*. New York, American Institute of Physics, 1984. *This book has several introductory chapters on the mathematics of ill-posed problems followed by several chapters on specific applications.*
15. Hansen PC. Analysis of discrete ill-posed problems by means of the  $L$ -curve. *SIAM Rev* 34(4):561, 1992. *This is an excellent review paper which describes the various techniques developed to solve ill-posed problems. Special attention is paid to the selection of the a priori approximation of the regularization parameter.*

16. Hansen PC, Regularization tools: A Matlab package for analysis and solution of discrete ill-posed problems. Available via netlib in the library numeralgo/no4. *This is an excellent set of tools for experimenting with and analyzing discrete ill-posed problems. The netlib library contains several Matlab routines as well as a postscript version of the accompanying technical report/manual.*
17. Yamashita Y. Theoretical studies on the inverse problem in electrocardiography and the uniqueness of the solution. *IEEE Trans Biomed Eng* 29:719, 1982. *The first paper to prove the uniqueness of the inverse problem in electrocardiography.*
18. Bertrand O. 3D finite element method in brain electrical activity studies. In J Nenonen, HM Rajala, T Katila (eds), *Biomagnetic Localization and 3D Modeling*, pp 154–171. Helsinki, Helsinki University of Technology, 1991. *This paper describes the inverse MEG problem using the finite-element method.*
19. Bowyer A. Computing Dirichlet tessellations. *Comput J* 24:162, 1981. *One of the first papers on the Delaunay triangulation in 3-space.*
20. Hoole SRH. *Computer-Aided Analysis and Design of Electromagnetic Devices*. New York, Elsevier, 1989. *While the title wouldn't make you think so, this is an excellent introductory text on the use of numerical techniques to solve boundary value problems in electrodynamics. The text also contains sections on mesh generation and solution methods. Furthermore, it provides pseudocode for most of the algorithms discussed throughout the text.*
21. MacLeod RS, Johnson CR, Matheson MA. Visualization tools for computational electrocardiography. In *Visualization in Biomedical Computing*, pp 433–444, 1992. *This paper and the paper which follows concern the modeling and visualization aspects of bioelectric field problems.*
22. MacLeod RS, Johnson CR, Matheson MA. Visualization of cardiac bioelectricity—A case study. *IEEE Visualization* 92:411, 1992.
23. Pilkington TC, Loftis B, Thompson JF, et al. *High-Performance Computing in Biomedical Research*. Boca Raton, Fla, CRC Press, 1993. *This edited collection of papers gives an overview of the state of the art in high-performance computing (as of 1993) as it pertains to biomedical research. While certainly not comprehensive, the text does showcase several interesting applications and methods.*
24. Thompson J, Weatherill NP. Structured and unstructured grid generation. In TC Pilkington, B Loftis, JF Thompson, et al. (eds), *High-Performance Computing in Biomedical Research*, pp 63–112. Boca Raton, Fla, CRC Press, 1993. *This paper contains some extensions of Thompson's classic textbook on numerical grid generation.*
25. George PL. *Automatic Mesh Generation*. New York, Wiley, 1991. *This is an excellent introduction to mesh generation. It contains a survey of all the major mesh generation schemes.*
26. Thompson JF, Warsi ZUA, Mastin CW. *Numerical Grid Generation*. New York, North-Holland, 1985. *This is the classic on mesh generation. The mathematical level is higher than that of George's book, and most of the applications are directed toward computational fluid dynamics.*
27. Schmidt JA, Johnson CR, Eason JC, MacLeod RS. Applications of automatic mesh generation and adaptive methods in computational medicine. In JE Flaherty and I. Babuska (eds), *Modeling, Mesh Generation, and Adaptive Methods for Partial Differential Equations*. New York, Springer-Verlag, 1994. *This paper describes three-dimensional mesh generation techniques and adaptive methods for bioelectric field problems.*
28. Henriquez CS, Johnson CR, Henneberg KA, et al. Large scale biomedical modeling and simulation: From concept to results. In N Thakor (ed), *Frontiers in Biomedical Computing*. Philadelphia, IEEE Press, 1994. *This paper describes the process of large-scale modeling along with computational and visualization issues pertaining to bioelectric field problems.*
29. Akin JE. *Finite Element Analysis for Undergraduates*. New York, Academic Press, 1986. *This is an easy-to-read, self-contained text on the finite-element method aimed at undergraduate engineering students.*

30. Johnson C. Numerical Solution of Partial Differential Equations by the Finite Element Method. Cambridge, Cambridge University Press, 1990. *An excellent introductory book on the finite-element method. The text assumes mathematical background of a first-year graduate student in applied mathematics and computer science. An excellent introduction to the theory of adaptive methods.*
31. Brebbia CA, Dominguez J. Boundary Elements: An Introductory Course. New York, McGraw-Hill, 1989. *This is an introductory book on the boundary element method by one of the foremost experts on the subject.*
32. Jawsom MA, Symm GT. Integral Equation Methods in Potential Theory and Elastostatics. London, Academic Press, 1977. *An introduction to the boundary integral method as applied to potential theory and elastostatics.*
33. Beer G, Watson JO. Introduction to Finite and Boundary Element Methods for Engineers. New York, Wiley, 1992. *This is an excellent first book for those wishing to learn about the practical aspects of the numerical solution of boundary value problems. The book covers not only finite and boundary element methods but also mesh generation and the solution of large systems.*
34. Johnson CR, MacLeod RS. Nonuniform spatial mesh adaption using a posteriori error estimates: Applications to forward and inverse problems. Appl Num Math 14:331, 1994. *This is a paper by the author which describes the application of the h-method of mesh refinement for large-scale two- and three-dimensional bioelectric field problems.*
35. Flaherty JE. Adaptive Methods for Partial Differential Equations. Philadelphia, SIAM, 1989. *This is a collection of papers on adaptive methods, many by the founders in the field. Most of the papers are applied to adaptive methods for finite-element methods and deal with both theory and applications.*
36. Golub GH, Van Loan CF. Matrix Computations. Baltimore, Johns Hopkins, 1989. *This is a classic reference for matrix computations and is highly recommended.*
37. Zienkiewicz OC. The Finite Element Method in Engineering Science. New York, McGraw-Hill, 1971. *This is a classic text on the finite-method. It is now in its fourth edition, 1991.*
38. Zienkiewicz OC, Zhu JZ. A simple error estimate and adaptive procedure for practical engineering analysis. Int J Num Meth Eng 24:337, 1987. *This is a classic paper which describes the use of the energy norm to globally refine the mesh based on a priori error estimates.*
39. Zienkiewicz OC, Zhu JZ. Adaptivity and mesh generation. Int J Num Meth Eng 32:783, 1991. *This is another good paper on adaptive methods which describes some more advanced methods than the 1987 paper.*
40. Burnett DS. Finite Element Method. Reading, Mass, Addison-Wesley, 1988. *This is an excellent introduction to the finite-element method. It covers all the basics and introduces more advanced concepts in a readily understandable context.*
41. Barber CB, Dobkin DP, Huhdanpaa H. The quickhull algorithm for convex hull. Geometry Center Technical Report GCG53. *A public domain two- and three-dimensional Delaunay mesh generation code. Available via anonymous ftp from geom.umn.edu:/pub/software/qhull.tar.Z. There is also a geometry viewer available from geom.umn.edu:/pub/software/geomview/geomview-sgi.tar.Z.*
42. Barr RC, Pilkington TC, Boineau JP, Spach MS. Determining surface potentials from current dipoles, with application to electrocardiography. IEEE Trans Biomed Eng 13:88, 1966. *This is the first paper on the application of the boundary-element method to problems in electrocardiography.*
43. Rudy Y, Messinger-Rapport BJ. The inverse solution in electrocardiography: Solutions in terms of epicardial potentials. CRC Crit Rev Biomed Eng 16:215, 1988. *An excellent overview on the inverse problem in electrocardiography as well as a section on the application of the boundary-element method to bioelectric field problems.*
44. Gulrajani RM, Roberge FA, Mailloux GE. The forward problem of electrocardiography. In PW Macfarlane and TD Lawrie (eds), Comprehensive Electrocardiology, pp 197–236. Oxford, England, Pergamon Press, 1989. *This contains a nice overview of the application of the boundary-element method to the direct ECG problem.*

45. Golub G, Ortega JM. Scientific Computing: An Introduction with Parallel Computing. New York, Academic Press, 1993. *An excellent introduction to scientific-computing with sections on sequential and parallel direct and iterative solvers, including a short section on the multigrid method.*
46. Freeman TL, Phillips C. Parallel Numerical Algorithms. New York, Prentice-Hall, 1992. *A good introduction to parallel algorithms with emphasis on the use of BLAS subroutines.*
47. Van de Velde EF. Concurrent Scientific Computing. New York, Springer-Verlag, 1994. *This text contains an excellent introduction to parallel numerical algorithms including sections on the finite-difference and finite-element methods.*