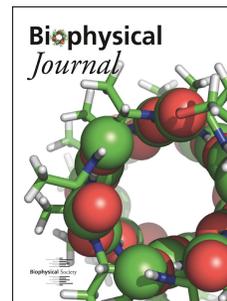


# Journal Pre-proof

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# Integrin-Based Mechanosensing through Conformational Deformation

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24 **Date:** 9/9/21

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**26 Abstract**

27 Conversion of integrins from low to high affinity states, termed activation, is  
28 important in biological processes including immunity, hemostasis, angiogenesis and  
29 embryonic development. Integrin activation is regulated by large-scale conformational  
30 transitions from closed, low affinity states to open, high affinity states. While it has been  
31 suggested that substrate stiffness shifts the conformational equilibrium of integrin and  
32 governs its unbinding, here we address the role of integrin conformational activation in  
33 cellular mechanosensing. Comparison of WT vs activating mutants of integrin  $\alpha_v\beta_3$   
34 show that activating mutants shift cell spreading, FAK activation, traction stress and  
35 force on talin toward high stiffness values at lower stiffness. Although all activated  
36 integrin mutants showed equivalent binding affinity for soluble ligands, the  $\beta_3$  S243E  
37 mutant showed the strongest shift in mechanical responses. To understand this  
38 behavior, we used coarse-grained computational models derived from molecular level  
39 information. The models predicted that wild type integrin  $\alpha_v\beta_3$  displaces under force,  
40 and that activating mutations shift the required force toward lower values, with S243E  
41 showing the strongest effect. Cellular stiffness sensing thus correlates with computed  
42 effects of force on integrin conformation. Together, these data identify a role for force-  
43 induced integrin conformational deformation in cellular mechanosensing.

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49 **Statement of Significance**

50           Cells sense extracellular matrix stiffness through integrins to regulate many  
51 functions. Despite extensive study, major questions about molecular mechanisms  
52 remain unanswered. Here, we report evidence that direct effects of force on integrin  
53 conformation determine cellular stiffness sensing. These results are conceptually  
54 important because they identify integrins as true mechanosensors that determine  
55 signaling outputs.

56

57

58

## 59 **Introduction**

60           Integrin-based adhesions are the primary structures through which cells sense  
61 and respond to the physicochemical properties of the extracellular matrix, including  
62 variations in stiffness, composition, topology and spatial distribution (1). The ability of  
63 integrin-based adhesions to respond to matrix stiffness is critical for many cellular  
64 processes, including cell division (2), migration (3, 4), embryogenesis (5) and wound  
65 healing (6), among others. Variations in the stiffness of the extracellular matrix affect the  
66 assembly, binding properties, clustering and stability of integrins and integrin-based  
67 adhesions, and govern cell spreading and traction force (1, 7). Dysregulation of  
68 mechanosensing from integrin-based adhesions is associated with a wide variety of  
69 disorders, including cardiovascular disease (8, 9), musculoskeletal dysfunction (10),  
70 fibrosis (11), and cancer (3).

71           Integrins are heterodimeric transmembrane receptors that bidirectionally transmit  
72 mechanical and biochemical signals. They specifically bind components of the  
73 extracellular matrix, with each integrin dimer exhibiting a specific repertoire of ligands.  
74 Integrins exist in a range of affinity states whose interconversion from inactive to active  
75 involves long range transitions from bent to extended conformations (12).  
76 Conformational activation can be regulated through both intracellular activators (i.e.  
77 Rap1, talin, kindlin) and through extracellular matrix ligands (i.e. fibronectin, collagen),  
78 thus providing tight control of integrin engagement with the extracellular matrix.

79           Force applied to integrins facilitates a transition from bent to extended  
80 conformation, and contributes to the maintenance of the active conformation (13).  
81 Application of force to already activated, ligand-bound integrins induces additional

82 recruitment of intracellular adaptor molecules, adhesion reinforcement and growth (1, 7,  
83 14, 15). Force on active, ligand-bound integrins also stabilizes the bound state,  
84 increases cellular traction force and spreading on surfaces, and activates downstream  
85 signaling pathways (16-18). These effects are generally attributed to transmission of  
86 force to talin, which then undergoes conformational transitions in which unfolding of  
87 helix bundle domains under tension triggers changes in binding partners, which both  
88 reinforces adhesions and regulates signaling (19). Other focal adhesion proteins such  
89 as p130Cas have also been proposed to function as direct mechanotransducers (20).

90         However, activating exogenous integrins with manganese ions increases cell  
91 spreading on soft surfaces that normally do not allow spreading (21). Integrin  $\alpha_v\beta_3$  is  
92 especially critical in cellular stiffness sensing (22). This integrin shows catch and then  
93 slip bond behavior as a function of force, where ligand-bond lifetimes for integrin  
94 increase with moderate force and then decrease at higher forces (23, 24). The idea that  
95 force either drives the conversion from inactive to active conformations or stabilizes the  
96 high affinity state, or both, suggests that integrin activation itself might play a role in  
97 mechanotransduction.

98         We therefore investigated the role of integrin conformation in stiffness sensing.  
99 Analysis of a collection of equivalently activated  $\alpha_v\beta_3$  mutants on elastic substrates of  
100 varying stiffness showed that these mutants shift cell spreading, activation of  
101 mechanosensitive signaling pathways (YAP, pFAK), traction forces and force on the  
102 central adhesion adaptor protein talin toward lower stiffness but to varying degrees. We  
103 then developed computational simulations based on coarse-grained modeling that  
104 utilize data from  $\mu$ s-long all-atom molecular dynamics simulations. The calculations

105 predict that the different mutants respond differently to force. Importantly, force-  
106 dependent transition to more extended conformations correlates closely with cellular  
107 stiffness sensing. These results identify a key role for force-induced integrin  
108 conformational deformation in cellular stiffness sensing.

109

## 110 **Methods**

### 111 **Cell culture, transfection**

112 Mouse lung endothelial cells (MLECs) isolated from  $\beta 3$  integrin null mice were  
113 generously provided by Mark Ginsberg and Brian Petrich (University of California at San  
114 Diego, CA) (25).  $\beta 3$  integrin single point mutants were generously provided by Timothy  
115 Springer (Harvard University, Boston MA) (26). These sequences were subcloned into  
116 pBOB vector and virus prepared in HEK 293Tx cells by co-transfecting with pCMV-VSV-  
117 G and psPAX2 using Lipofectamine 2000 (Invitrogen). The temperature sensitive  
118 mutant of the SV40 virus large T antigen was employed for conditional immortalization  
119 of these cells. Immortalized  $\beta 3^{-/-}$  MLECs were infected with wild-type (WT) or mutant  
120  $\beta 3$  integrin viruses and subsequently sorted to obtain homogenous populations with  
121 equal expression levels (24). For expansion, MLECs were cultured in 1:1 Hams F-12  
122 and high glucose DMEM with 20% FBS, 1% Penicillin-Streptomycin, 2.5mM glutamine  
123 and endothelial cell growth supplement (ECGS, 50mg/L) at the permissive temperature  
124 of 30°C. For experiments, cells were switched to 37°C to inactivate large T one day  
125 prior.

### 126 **Polyacrylamide Substrate Preparation**

127 Small polyacrylamide gels for imaging experiments were prepared as described  
128 (27). Briefly, 20mm coverslip bottom dishes (Mattek) were silanized with a 2% solution  
129 of 3-aminopropyltrimethoxysilane in isopropanol for 10 minutes at room temperature.  
130 After washing with ddH<sub>2</sub>O and drying, coverslips were incubated with 1%  
131 glutaraldehyde solution in ddH<sub>2</sub>O for 30 minutes and then washed 3 times.  
132 Polyacrylamide gels were cast onto the silanized surface by preparing acrylamide/bis-  
133 acrylamide solutions (Biorad) of various ratios (Supplemental Table 1) and polymerizing  
134 with ammonium persulfate (American bio) and TEMED (Sigma). Gels were cast  
135 between the silanized surface and a 12mm uncoated glass coverslips with a volume of  
136 8ul. After casting, gels were treated with fresh sulfo-SANPAH (Sigma) in ddH<sub>2</sub>O  
137 (2mg/ml) and exposed to UV light for 3 minutes (8W, 254 nm wavelength at a distance  
138 of 2-3 inches). After UV, gels were washed with ddH<sub>2</sub>O and then covered with  
139 fibrinogen (200ug/ml in PBS at pH 7.4) overnight at 4°C. Prior to seeding, gels were  
140 washed 3 times with PBS and pre-incubated with medium for 1 hour. Cell spreading  
141 experiments were performed in serum free conditions to prevent fibronectin deposition  
142 (High Glucose DMEM (Gibco) with 0.5% w/v bovine serum albumin (sigma), 1x Insulin-  
143 Transferrin-Selenium (ITS premix, Gibco)).

144 Larger polyacrylamide gels for western blot experiments were prepared using a  
145 modified version of the protocol from Elosegui A., et al (28). Briefly, 35-mm glass  
146 bottom dishes were activated with glacial acetic acid, 3-(trimethoxysilyl) propyl  
147 methacrylate, and 96% ethanol solution (1:1:14 ratio, respectively) for 10 minutes in  
148 room temperature. For fibrinogen conjugated gels, acrylamide was partially replaced  
149 with acrylic acid N-hydroxysuccinimide ester according to Supplemental Table 2, as

150 derived from (28). Cast gels were coated with fibrinogen (200ug/ml in PBS pH7.4)  
151 overnight at 4°C. Cells were plated in serum free medium (High Glucose DMEM (Gibco)  
152 with 0.5% w/v bovine serum albumin (Sigma), 1x Insulin-Transferrin-Selenium (ITS  
153 premix, Gibco) to prevent FN deposition.

154

### 155 **Cell Immunostaining and Quantification**

156 Cells seeded on fibrinogen-coated glass or polyacrylamide were fixed with 4%  
157 paraformaldehyde (Electron Microscopy Sciences) in PBS. Cells were washed and  
158 permeabilized with 0.05% Triton X-100 in PBS supplemented with 320 mM sucrose and  
159 6 mM MgCl<sub>2</sub>, then washed 3 times with PBS and blocked for 30 minutes with 1% BSA in  
160 PBS. Cells were incubated overnight at 4°C with anti-YAP antibody (1:200, catalog  
161 number sc-101199, Santa Cruz Biotechnology) diluted in 1% BSA in PBS. Cells were  
162 washed 3 times with PBS and incubated at room temperature for 1 hour with secondary  
163 antibody (Alexa-647 anti-mouse, 1:1000, Molecular Probes) and Alexa-565 conjugated  
164 phalloidin (1:1000, Molecular Probes). They were washed again 3 times with PBS and  
165 mounted with DAPI in Fluoromount-G (Southern Biotech). Cell areas were quantified  
166 using ImageJ by background subtracting, thresholding to generate cell masks, and  
167 using the analyze particles function. YAP nuclear to cytosolic ratios were quantified by  
168 masking nuclear areas (DAPI) and cell areas (phalloidin) of interest in imageJ and then  
169 dividing the background-subtracted average signal in the nucleus by the average signal  
170 in the cytoplasm using MATLAB (Mathworks).

171

### 172 **qPCR**

173 Relative expression of CTGF versus  $\beta$ -actin was determined by rtPCR with  
174 primers for mouse actin (fw: 5'-cgagcgtggctacagcttc-3'; rv: 5'-gccatctcctgctcgaagtc-3'),  
175 and mouse CTGF (fw: 5'-ctgcagactggagaagcaga-3'; rv: 5'-gatgcacttttgccttctt-3'). Cells  
176 were cultured on soft (3kPa) or stiff (30kPa) fibrinogen coated silicone gels for 24 hours  
177 in serum free media with fibronectin blocking antibody (16G3, 25ug/ml) with fresh  
178 antibody added at 0 and 12 hours to prevent cell deposited fibronectin from interfering.  
179 mRNA was isolated at 24 hours by directly lysing cells on the gel surface using the  
180 mRNeasy kit (Qiagen) and cDNA was synthesized using iScript cDNA synthesis kit  
181 (Biorad). PCR was run for 40 cycles on a Biorad CFX96 rtPCR machine using  
182 SsoAdvanced universal SYBR green supermix (Biorad).

183

#### 184 **Western Blot**

185 MLECs seeded on PA gels were lysed directly in SDS sample buffer (100mM  
186 Tris-Cl pH6.8, 4% SDS, 0.2% Bromophenol Blue, 20% glycerol) with protease and  
187 phosphatase inhibitors (Halt protease inhibitor cocktail 100x, Thermo) and 2.5% beta-  
188 mercaptoethanol. Lysates were sonicated for 30 seconds and boiled at 95°C for 5  
189 minutes. Samples were loaded onto 8% or 10% SDS-PAGE gels and run for 90  
190 minutes at 120V in Tris-glycine buffer with SDS. Transfer was performed using Tris-  
191 Glycine 20% Methanol buffer onto nitrocellulose membranes (Biorad) with a Transblot  
192 Turbo (Biorad). Membranes were blocked with 5% BSA in Tris-buffered saline with  
193 0.1% Tween 20 in 150mM NaCl, 50mM Tris-HCl, pH 7.6 (TBS-T) for 1 hour.  
194 Membranes were incubated overnight at 4°C with primary antibodies directed at total  
195 FAK (cell signaling 1:1000) or phosphorylated FAK (Y397, Cell Signaling, 1:1000) in

196 TBS-T. Membranes were washed 3 times for 5 minutes with TBS-T and incubated for 1  
197 hour at room temp with peroxidase-conjugated anti-mouse or anti-rabbit secondary  
198 antibodies (1:4000 in TBS-T, vector labs). Membranes were washed 3 times for 5  
199 minutes and bands were detected using Supersignal West Pico PLUS or Fempto  
200 detection reagents (Thermo) and imaged on a G:BOX gel imager (SYNGENE).

201

## 202 **Traction Force Microscopy**

203 Silicone TFM substrates were fabricated as described (29). Briefly, cover-glass  
204 bottom 96 well plates were spin-coated with a ~40 $\mu$ m thick layer of a silicone gel pre-  
205 polymer polydimethylsiloxane (CY 52-276 by Dow Inc., mixed at various A:B ratios,  
206 1.4kPa = 0.8:1; 3.1kPa = 0.9:1; 11kPa = 1.2:1; 1.6:1 30kPa). Gel pre-polymer is cured  
207 by baking at 70°C overnight then treated with 3-aminopropyl trimethoxysilane for 5 min  
208 and incubated for 10 min at room temperature under a suspension of 40nm Alexa Fluor  
209 647 beads (molecular probes) in a 100 $\mu$ g/ml solution of 1-Ethyl-3-(3-  
210 dimethylaminopropyl) carbodiimide (EDC, Sigma) in water to covalently link beads to  
211 the gel surface. Gel modulus for each batch was measured using a microfluidic device  
212 (29) and is reported as Young's elastic modulus (E).

213 TFM gels were coated with fibrinogen (10 $\mu$ g/ml) in PBS overnight at 4°C. Prior to  
214 seeding, gels were washed 3 times with PBS. Traction force experiments were  
215 performed in serum free conditions to limit fibronectin deposition (Phenol-Free High  
216 Glucose DMEM (gibco) with 0.5% w/v bovine serum albumin (Sigma), 1x Insulin-  
217 Transferrin-Selenium (ITS premix, gibco), and 1 $\mu$ M lysophosphatidic acid (Sigma). The  
218 day of the experiment, cells were trypsinized and seeded on TFM substrates at low

219 density (~3000 cells per cm<sup>2</sup>) for 2 hours. Cells and fluorescent beads were imaged on a  
220 spinning disk confocal microscope (UltraVIEW VoX, Perkins Elmer) attached to a Nikon  
221 A-1 microscope equipped with a temperature and CO<sub>2</sub> controlled incubation chamber  
222 and 60x 1.4NA lens. Fluorescent images of Alexa Fluor 647 beads and DIC images of  
223 cells were acquired before and after cell lysis with 0.05% SDS. Images were drift  
224 corrected and bead displacements were quantified using a previously developed open  
225 source traction force microscopy software in MATLAB 2015a (26). Force fields and  
226 traction stresses were calculated using FTTC force reconstruction with regularization  
227 parameter set at (1kPa = 0.01, 3.1kPa = 0.001, 11kPa = 0.0001, 31kPa = 0.00005).  
228 Regularization parameter was chosen to give smooth traction maps and a single  
229 parameter was used for all groups at a given stiffness. Average stress per cell was  
230 calculated as the total force for a cell divided by its spread area.

231

### 232 **FRET Imaging and Quantification**

233 Quantification of FRET data was performed using the custom software in  
234 MATLAB we developed previously (30). All three FRET images (eGFP, tagRFP, FRET)  
235 were corrected for illumination gradient, pixel shift and background subtraction, followed  
236 by three-point smoothing. Bleed through and cross excitation co-efficients were  
237 calculated by imaging cells transfected with eGFP-talin or tagRFP-talin. The slope of  
238 the pixel-wise donor or acceptor channel intensity versus FRET channel intensity gives  
239 bleed through (x) or cross-excitation (y) fraction, respectively. Heat maps of FRET and  
240 pixel-wise FRET index were calculated using the following equation:

$$FRET\ Index = \frac{FRET - x(GFP) - y(RFP)}{RFP}$$

241 where FRET, GFP, and RFP are the shade, shift and background corrected pixel  
242 intensities for each of the respective channels. Average FRET Index was calculated for  
243 masked focal adhesions in each cell. Focal adhesion sizes for Talin tension sensor  
244 images were quantified using the focal adhesion analysis server (FAAS) (31) with  
245 default settings for static properties only and for adhesions greater than  $0.2\mu\text{m}^2$ .

246

### 247 **Computational Models of Active $\alpha_V\beta_3$ Integrin under Force**

248 We used a CG computational model in order to study the effect of force on wild  
249 type  $\alpha_V\beta_3$  integrin and the L138I, K417E, and S243E mutants. Starting from  $\mu\text{s}$ -long  
250 equilibrium all-atom molecular dynamics simulations, we decreased the representation  
251 of each integrin from 1780 C $\alpha$  atoms to 300 CG beads (average resolution  $8 \pm 4$  C $\alpha$   
252 atoms per CG bead), using the Essential Dynamics Coarse Graining approach (32).  
253 Each CG bead of bent  $\alpha_V\beta_3$  was placed at the center of geometry of the corresponding  
254 C $\alpha$  atoms of open  $\alpha_{IIB}\beta_3$  integrin (33). Then, CG beads were connected using effective  
255 harmonic and Morse interaction potentials by applying our recent hENM-based  
256 approach (for details, see (34) and SI). Lastly, we ran Langevin Dynamics using the  
257 molecular dynamics software LAMMPS (35), with the temperature set at 310 K, with a  
258 constant number of particles, volume, and temperature (NVT) ensemble. In order to  
259 mimic the effect of the cell membrane, transmembrane helices were spatially restrained;  
260 to mimic the effect of substrate rigidity, a pulling force was applied on the ligand binding  
261 site. For outputs, we analyzed structural parameters representative of conformational  
262 stability of integrin, including overall integrin length and separation between the two  
263 integrin legs.

264

**265 Backmapping of Coarse-grained to All-atom models**

266 The initial atomic model for WT integrin was constructed from structures obtained via x-  
267 ray crystallography and solution NMR (3IJE.pdb (36) and 2KNC.pdb (37)). Missing  
268 amino acid backbones were built using MODELLER (38), and missing side chains were  
269 optimized using SCWRL4 (39). In the all-atom model of integrin, center-of-mass (COM)  
270 positions of atoms belonging to each CG particle were computed of the unloaded CG  
271 system. The COM positions were grouped on the basis of distinct secondary structural  
272 elements of the protein. For each secondary structural element, rotation and translation  
273 matrices were computed by minimizing the RMSD in a rigid-body fit of the COM  
274 positions to the CG conformation of WT integrin derived from the CG MD simulations  
275 without force. These transformation matrices were then applied to the corresponding all-  
276 atom model for each secondary structural element to generate an initial backmapped  
277 model (Sup. Fig. 5A-B). The backmapped all-atom structures were subsequently refined  
278 using steepest descent and adopted basis Newton Raphson energy minimization  
279 algorithms in the CHARMM36 force field (40, 41). The same backmapping procedure  
280 was repeated for the S243E integrin mutant and the corresponding CG conformation  
281 derived from the CG MD simulations. The backmapped all-atom structures were  
282 inserted into a lipid bilayer with 80% DOPC and 20% DOPS lipids (960 lipids in each  
283 leaflet, total 1920 lipids in membrane) using CHARMM-GUI membrane builder (33).  
284 Similar to the initial AA MD simulations, the lipid-membrane/integrin systems were  
285 hydrated with TIP3P water molecules and 150 mM NaCl, for a total of about 1.9 million  
286 atoms for wild type integrin and 2.2 million atoms for S243 mutant. The sizes of these

287 systems were significantly larger than the initial AA systems, owing to the more  
288 extended and open configurations of stretched integrin, which occupy a larger volume in  
289 the computational domain. Energy minimization was run for 5000 steps of steepest  
290 descent algorithm, then equilibration was performed to relax the system. We used a six-  
291 step protocol where decreasing restraints were applied to the protein, lipids and water  
292 molecules: NVT dynamics (constant volume and temperature) was used for the first two  
293 steps, followed by NPAT dynamics (constant pressure, area and temperature) for the  
294 rest, at 310 K. At the end of equilibration, we analyzed structural properties of AA wild  
295 type and S243 mutant integrins. Consistent with the structural properties of the  
296 stretched coarse-grained structures, comparison of stretched wild type integrin to the  
297 S243E mutant showed a more bent headpiece (122 deg +/- 7.8 deg for WT genu angle  
298 vs 166 deg +/- 18.3 for S243E) and closer chains (genu separation 7.6 nm +/- 0.4 nm for  
299 WT vs 4.7 nm +/- 1.1 nm for S243E), see Fig 5C-D. Constant-force steered MD was  
300 done on the backmapped all-atom systems and revealed that the S243E mutant  
301 extended more than WT under force (Fig. 5E-F). These results indicate that the  
302 structural properties of the CG systems are maintained at the molecular levels in  
303 stretched integrins and provide further evidence that force stabilizes extended integrin  
304 conformations.

305

### 306 **Steered Molecular Dynamics of Backmapped All-atom integrin models**

307 In order to evaluate the effect of an external force on the extension of all-atom integrin,  
308 we performed Steered Molecular Dynamics simulations (SMD) on the backmapped and  
309 energy minimized AA wild type and S243 mutants. A constant vertical force of 1 or 10

310 pN was applied to the center of mass of the ligand binding site, while the  $\beta$  chain  
311 transmembrane helix was held fixed within the lipid bilayer. The simulations were  
312 performed using Gromacs 5.0.4 (42), for 500 ps in the NPT ensemble using Berendsen  
313 barostat (43), keeping the temperature at 310 K and pressure at 1 atm with semi-  
314 isotropic pressure coupling with a compressibility of  $4.5 \times 10^{-5} \text{bar}^{-1}$ . Long-range  
315 electrostatic interactions were incorporated through the Particle Mesh Ewald (PME)  
316 method with a cut-off of 1 nm (44). Analysis of extension at 1 pN or 10 pN constant force  
317 was performed.

318

319

## 320 **Statistics**

321 All of the statistical analysis was performed using Prism version 7.01 (Graphpad).  
322 Details regarding the specific statistical tests used, the sample size, p values, and  
323 number of independent experiments are provided in the figure legends. All  
324 experimental data are included in the supplemental data spreadsheet. Modeling results  
325 are available at [https://github.com/tamarabidone/integrins\\_AA\\_CG](https://github.com/tamarabidone/integrins_AA_CG).

326

## 327 **Results**

### 328 **Activating mutants drive cell spreading on soft substrates**

329 To assess the effects of activating mutations on stiffness sensing, we expressed  
330 wild type  $\beta 3$  integrin or activated mutants (L138I, S243E, K417E) (45) in immortalized  
331  $\beta 3$  integrin knockout mouse lung endothelial cells (MLECs). Previous studies used  
332 binding to the monomeric high affinity soluble ligand WOW-1 as the optimal assay for

333 integrin affinity without interference from clustering and in the absence of force (46).  
334 These results showed that the mutations resulted in increased affinity that was  
335 indistinguishable between the mutants (34). To assess spreading and YAP nuclear  
336 localization as typical stiffness-dependent functions, polyacrylamide gels of varying  
337 stiffnesses were coated with the  $\beta 3$  ligand fibrinogen.  $\beta 3^{-/-}$  cells show minimal adhesion  
338 to these surfaces, demonstrating specificity. Cells expressing equivalent levels of wild  
339 type (WT) or mutant  $\beta 3$  were plated and assayed at 3 hours to minimize fibrinogen  
340 proteolysis or other modifications of the substrates. WT  $\beta 3$  cells adhered well and  
341 showed the expected stiffness-dependent increase in spread area and YAP nuclear  
342 localization (Fig. 1A,B and Sup. Fig. 1). Activating mutations shifted the ability of cells  
343 to spread and induce YAP nuclear localization toward lower stiffnesses (Fig. 1A-C).  
344 Interestingly, L138I had only a weak effect whereas S243E and K417E strongly shifted  
345 the behavior toward softer substrates without increasing maximal cell spreading or YAP  
346 nuclear localization on stiff substrate. These results were confirmed by quantification of  
347 the YAP target gene CTGF (Sup. Fig. 2A), which showed increased expression for all  
348 mutants on soft (3kPa) gels. Integrin activation thus promotes spreading on soft  
349 substrates, confirming the results with  $Mn^{2+}$  activation of integrin (21). Additionally, our  
350 results show that the mechanosensitive YAP pathway is similarly regulated.

351

### 352 **Activating mutants and tyrosine phosphorylation**

353 We next assessed phosphorylation of focal adhesion kinase (FAK) on tyrosine  
354 397, a well-established mechanosensitive event, in cells plated on gels of different  
355 stiffness. As expected (47, 48), cells expressing WT  $\beta 3$  showed increasing pFAK (Fig.

356 2A-B) with increasing stiffness. All of the activating  $\beta 3$  mutations showed non-  
357 significant trends toward higher phosphorylation of FAK (Fig. 2B) in suspension, which  
358 we take as the baseline levels. Importantly, the S243E mutant showed a large and  
359 significant increase in pFAK/tFAK at low stiffness (0.5kPa) (Fig. 2B). We also analyzed  
360 these curves by calculating the effective stiffness required for 50% maximal FAK  
361 activation, YAP nuclear translocation, and cell spreading (ES50 for these variables).  
362 This metric revealed downward shifts in the threshold for stiffness-dependent activation  
363 for all mutants, with S243E having the most consistent and largest effect for all three  
364 outputs (Sup. Fig. 2B). While this approach provides a simple, convenient way to  
365 quantify the shift in stiffness sensitivity, it may underestimate the actual difference due  
366 the fact that the WT group did not reach saturation at the highest stiffness values.

367

### 368 **Activating mutants and traction force**

369 To assay the mechanical forces at the cellular length scale, we measured  
370 traction stresses as a function of substrate stiffness (1.4, 3.1, 11, 31 kPa). Cells plated  
371 on fibrinogen-coated silicone gels containing fluorescent beads were imaged before and  
372 after cell lysis. Cell-induced bead deformations were analyzed to generate heatmaps of  
373 traction stress (Fig. 3A, Sup. Fig. 3A-D) which were cropped for the area occupied by  
374 the cell to calculate average traction stress per cell (Fig. 3B). Measurements were  
375 performed 2 hours after seeding, when traction forces stabilize but are specific to  $\beta 3$   
376 integrin (Sup. Fig. 2C). Cells expressing WT  $\beta 3$  showed increasing traction stress with  
377 increasing stiffness, as expected (28). The L138I and K417E mutants showed only  
378 slightly elevated stresses at the intermediate stiffnesses (Fig. 3B). By contrast, the

379 S243E mutant showed maximal traction stress at low stiffness with no further increase  
380 (Fig. 3B). Traction forces are well known to increase as a function of cell spreading  
381 (49). Reporting these values as stress, which is force per unit area, partly accounts for  
382 this effect. That traction stresses for the L138E and K417E mutants are not significantly  
383 different from WT  $\beta$ 3 indicates that their increased cell spreading on soft substrates  
384 largely accounts for the resultant increase in traction force. By contrast, S243E  
385 significantly increasing traction stress, especially at low stiffness, meaning that the  
386 increase in force is greater than what would be expected for the increased spreading.

387 With accumulating evidence that the S243E mutation uniquely influences forces  
388 at the cellular scale, these effects might conceivably be due to recruitment of a greater  
389 number of activated integrins to the adhesions. To exclude such effects, we used a  
390 previously developed FRET-based tension sensor which uses a FRET pair (eGFP and  
391 mRFP) separated by an elastic peptide linker that reports force/molecule (50). To  
392 assay force on talin, the central focal adhesion protein that links integrins to F-actin, we  
393 used the previously characterized tension sensor in which the module was inserted  
394 between the head domain that binds the integrin  $\beta$  tail and the rod domain that binds F-  
395 actin (30). Force on talin results in separation of the FRET pair and decreased FRET  
396 efficiency. These results were compared to the control FRET sensor (CTS) in which the  
397 module is fused to the C-terminus; this construct localizes similarly but is not exposed to  
398 force. A previous study (30) validated the force-sensitivity of the probe and showed that  
399 force on talin is diminished on soft substrates. We simultaneously measured force on  
400 talin (FRET index) and average traction stress (Fig. 3C) on soft (1.4kPa) silicone gels in  
401 the same cells. The S243E mutant showed the highest traction stress (Fig. 3D) and the

402 lowest FRET index (Fig. 3E, Sup. Fig. 2G), indicating the highest force on talin. On  
403 glass, which is very stiff, there was a trend toward higher talin tension in S243E cells but  
404 it did not reach significance (Sup. Fig. 2D and 2E). Measurement of focal adhesion size  
405 showed that the S243E displayed larger talin adhesions on soft gels but similar focal  
406 adhesion sizes on glass (Sup. Fig. 2D and 2F). Together, multiple assays indicate that  
407 the S243E activating mutation induces high stiffness responses on soft gels, thus,  
408 appears to sensitize cells to low forces.

409

### 410 **Computational analysis of Integrin mechanical properties**

411 To investigate how integrin activating mutations alter stiffness sensing at the  
412 length scale of individual integrins, we built computational simulations using a coarse-  
413 grained (CG) modeling approach built “bottom-up” from all-atom molecular dynamics  
414 data converted into hetero-elastic network models (hENM) (Fig. 4A-B) (51). Integrins  
415 were represented by CG “beads” representing groupings of amino acids interconnected  
416 by effective harmonic and anharmonic potentials (Fig. 4B), according to our recently  
417 developed method (34). Force,  $F$ , was applied to the ligand binding site in the  $\beta$   
418 headpiece (Fig. 4B) and the subsequent changes for each mutant were evaluated (Fig.  
419 4C). We first used  $F = 0$  pN as the starting point and  $F = 1$  pN to mimic soft  
420 substrates/low force. Although catch bond behavior has not been analyzed for integrin  
421 avb3, studies of LFA1 (aLb2) detected catch bond in the low pN range (52), similar to  
422 the values used here. Simulations were then run for 1  $\mu$ s. The root means square  
423 displacement (RMSD) of the integrin, computed as the averaged displacement of all the  
424 beads, was then evaluated for each mutant. All of the activating mutants exhibited

425 increased displacement (movement away from the starting positions during the  
426 simulation) under this low force compared to WT, with the difference being somewhat  
427 higher for S243E relative to the other mutants (Fig. 4D). S243E also presented  
428 significantly lower elastic constants and equilibrium separations between CG beads  
429 (Sup. Fig. 4A-C), resulting in higher conformational flexibility (Sup. Fig. 4D) and  
430 headpiece fluctuations (Sup. Fig. 4E). Under 0 or low (1 pN) force, the mutant integrins  
431 were more extended than wild type, with the mutant S243E showing the largest effect  
432 (Fig. 4E). At higher forces (3 and 5pN), all constructs showed significant increases in  
433 RMSD (Fig. 4D).

434         Integrin activation at the ligand binding site is communicated to the cytoplasmic  
435 domains via a long-range conformation change that separates the legs of the  $\alpha$  and  $\beta$   
436 subunits, leading to intracellular signaling (53). Separation of the legs is thus linked to  
437 activation. This distance, measured at the genu region, was highest for S243E under 0  
438 pN force and did not increase further (Fig. 4F and Sup. Fig. 4D), consistent with the  
439 increased signaling under conditions of low force. S243E also showed increased force-  
440 extension relations (Sup. Fig. 4F-G). To assess the validity of the tension-dependent  
441 CG configurations, we backmapped wild type and S243E into atomistic models, which  
442 were energy minimized and equilibrated with all-atom MD in lipid membranes, then  
443 subjected to constant-force steered molecular dynamics simulations. These structures  
444 exhibited no steric clashes between lateral chains (Fig. 5A-D) and S243E integrin  
445 extended more than wild type under force (Fig. 5E-F). Together, these results show  
446 that the activating integrin mutant S243E is uniquely responsive to soft substrates due  
447 to its enhanced protein extension and flexibility under low forces.

448

449 **Discussion**

450           The ability of cells to sense the mechanical properties of their extracellular matrix  
451 through integrins is critical for cell differentiation, migration, tissue mechanical  
452 homeostasis and other functions (1-6). Due to their critical role in creating the physical  
453 link between cells and extracellular matrix, integrins are a key component of matrix  
454 mechanosensing (1, 15). But whether integrins are true mechanotransducers, that is,  
455 proteins whose conformational transitions under force are critical to signaling, is  
456 unknown. Published work has focused on talin (28), vinculin (16), FAK (47) , YAP (54),  
457 or integrin type (17) as the main determinant of stiffness sensing and  
458 mechanotransduction. However, it is known that integrin-ligand bonds stabilize under  
459 moderate forces, exhibiting so-called catch bond behavior (23). A previous study using  
460 manganese to activate integrins suggested a role for integrin activation in stiffness  
461 sensing (21), We therefore investigated the role of integrin conformation in  
462 mechanosensing in greater detail.

463           Here, we report a correlation between integrin conformational flexibility at the  
464 single molecule level and cellular stiffness sensing. For the endothelial cells used in  
465 this study, the transition in spreading, traction force and signaling is centered around 3-  
466 5 kPa, with those functions reaching a plateau above ~10 kPa, similar to published data  
467 for other adherent, well spread cell types (28, 47, 48). We also show that downstream  
468 mechanosensory pathways are impacted by this activation on soft gels, directly  
469 implicating integrin activation as a “mechanosensor”. However, examination of several  
470  $\beta 3$  mutants revealed distinct effects on cellular mechanosensing that cannot be  
471 explained by differences in simple binding affinity, i.e., in the absence of force. Instead,

472 the S243E mutant had strong effects in multiple assays despite an equivalent increase  
473 in binding of soluble ligand (34).

474         Understanding these results requires analysis of effects of force on integrin  
475 conformation. However, this goal is not experimentally accessible. We therefore used  
476 our recently developed CG simulation approach to address how integrin conformation  
477 changes under tension. The benefit of the CG model is its ability to sample large  
478 conformational changes by explicitly incorporating breakage of effective bonds between  
479 CG beads from atomistic fluctuations. By taking interaction parameters directly from all-  
480 atom molecular dynamics simulations, our hENM-based CG model implicitly  
481 incorporates the effects of single point mutations on residue motions into the strength  
482 and functional forms of the interactions between beads in the CG systems.  
483 Consequently, when force is applied between the ligand binding site and the  
484 cytoplasmic domain, all CG integrins examined here extend and rearrange their beads  
485 on the headpiece chains relative to lower legs. In particular, WT  $\alpha v\beta 3$  extended,  
486 consistent with increased activation of integrins under tension. By contrast, all of the  
487 activating mutations increased length in the absence of tension ("resting" length) with  
488 further increases upon application of tension, with the S243E mutant showing the  
489 largest effect. It is noteworthy that both experimental and simulation data show that the  
490 mutations induce a leftward shift in the force-dependence, which is greatest for S243E.

491         Together, these results provide evidence that integrin conformational activation is  
492 not only force dependent but imparts mechanosensitivity that determines multiple  
493 signaling outputs, including cell spreading, YAP and FAK activation and exertion of  
494 traction force. These effects fit well with the widely accepted model in which early

495 integrin outside-in signaling promotes adhesion reinforcement to amplify subsequent  
496 events such as activation of tyrosine kinases, RhoA and cell contractility, which increase  
497 additional downstream signals such as Yap/Taz (55, 56). These findings thus indicate  
498 that integrin  $\alpha v \beta 3$  is a true mechanosensor. Many studies have implicated integrins in  
499 mechanosensory processes and previous modeling work has identified that force  
500 accelerates hinge-angle opening from inactive to active states (57). However, the  
501 importance of force induced deformation of the active and ligand bound integrin in  
502 mechanosensing, meaning regulation of signaling pathways, has not to our knowledge  
503 been previously demonstrated.

504         Although not accessible by the methods used here, it seems likely that integrin  
505 catch bond behavior plays a significant role in these processes. Thus, the S243E  
506 mutant may convert to high affinity or long lived states at lower force thresholds. In any  
507 case, bond lifetime information must be relayed to the cell interior to regulate signaling  
508 pathways. Integrins are well suited for this function as conformational effects are  
509 transmitted over long distances to the cytoplasmic domain. Leg separation distance  
510 may also be an important regulator of intracellular binding and our modeling results  
511 indicate that the S243E mutant has the largest leg separation distance at 0 and 1 pN  
512 applied force. The interaction with talin is an obvious candidate but contributions from  
513 other proteins that interact with integrin cytoplasmic domains are also likely. The ILK-  
514 PINCH-parvin complex and kindlins are also implicated in mechanosensing and could  
515 thus mediate effects. Understanding how alterations in integrin conformation affect both  
516 extracellular and intracellular binding interactions is the major direction for future work.

517

518 **Author contributions:** M.A.S., G.A.V., T.P.D., and T.C.B designed the research;  
519 T.P.D., T.C.B., and S.A. performed the research; T.P.D., T.C.B, A.G., and G.A.V.  
520 contributed new reagents/analytic tools; T.P.D. and T.C.B. analyzed the data; A.Y. and  
521 T.C.B. performed the backmapping. T.P.D., T.C.B and M.A.S. wrote the paper.

522

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546 **Figure Legends**

547

548 **Figure 1: Integrin activating mutants increase spreading and YAP nuclear**549 **localization at low stiffness.**

550 **(A)** Cell spread area 3 hours after seeding on fibrinogen-coated polyacrylamide of the  
551 indicated Young's Modulus. Area was quantified from area of phalloidin-stained  $\beta 3$  KO  
552 MLECs reconstituted with the indicated  $\beta 3$  Integrin. Values are means  $\pm$  SEM, n= 25-123  
553 Cells per group from two independent experiments, \*  $p < 0.05$ , \*\*  $p < 0.01$ , \*\*\*  $p < 0.001$ , #  
554  $p < 0.05$  vs WT at same stiffness, two-way ANOVA with Tukey's post hoc (KO cells  
555 n=10-25 due to limited adhesion). **(B)** Quantification of the ratio of nuclear to  
556 cytoplasmic YAP signal at each stiffness. Values are means  $\pm$  SEM, n=25-123 cells per  
557 group from two independent experiments, \*  $p < 0.05$ , \*\*\*  $p < 0.001$ , two-way ANOVA with  
558 Tukey's post hoc. **(C)** Representative images of F-Actin (Phalloidin), YAP, and DAPI  
559 staining for MLECs on 0.6kPa gels (scale bar = 50 $\mu$ m)

560

561 **Figure 2: FAK phosphorylation.**

562 **(A)** Western blots for phosphorylated FAK (Y397) normalized to total FAK on fibrinogen-  
563 coated polyacrylamide gels of the indicated stiffness (S= suspension) for  $\beta 3$  KO MLECs  
564 reconstituted with WT or mutant  $\beta 3$  Integrin (L138I, S243E, K417E activating  
565 mutations). **(B)** Densitometry of phosphorylated FAK normalized for total FAK. Values  
566 are means  $\pm$  SEM, n=4 independent experiments, #  $p < 0.05$ , one-way non-parametric  
567 ANOVA with Dunn's multiple comparison.

568 **Figure 3: Traction stresses and force on talin.**

569 **(A)** Heat maps for traction stress for MLECs with WT or mutant  $\beta 3$  integrin on  
570 fibrinogen-coated silicone surfaces of the indicated stiffness. Surfaces were coated with  
571 fluorescent beads (Alexa-647) and bead displacements were tracked before and after  
572 cell lysis for calculation of stresses which were cropped for the area of the cell (outlined  
573 in yellow, scale bar =  $10\mu\text{m}$ ). **(B)** Quantification of average traction stress per cell for  
574 WT and mutant reconstituted cells. Values are means  $\pm$  SEM,  $n=33-41$  cells per group  
575 from 3 independent experiments, \*\*  $p<0.01$ , \*\*\*  $p<0.001$ , \*\*\*\*  $p<0.0001$ , two-way  
576 ANOVA with Dunnett's multiple comparison). **(C)** Heat maps of traction stress (left) and  
577 FRET index of talin tension sensor (middle) with images of GFP-talin focal adhesions  
578 (right) for experiments with simultaneous measurement of traction force and force on  
579 talin on soft fibrinogen coated silicone surfaces ( $1.4\text{kPa}$ ) (scale bar =  $10\mu\text{m}$ ). **(D)**  
580 Quantification of average traction stress per cell. Values are means  $\pm$  SEM,  $n=7-10$  cells  
581 per group from two independent experiments, ##  $p=0.0119$ , one-way ANOVA with  
582 Dunnett's multiple comparison). **(E)** Quantification of average FRET index per cell.  
583 Values are means  $\pm$  SEM,  $n=7-10$  cells per group from two independent experiments, #  
584  $p=0.0286$ , ##  $p<0.001$ , one-way ANOVA with Dunnett's multiple comparison, CTS  
585 indicates talin C-terminal control sensor expressed in WT cells).

586

587 **Figure 4. Computational analysis of integrin conformation.**

588 **(A)** Ribbon representation of bent integrin, with point mutations in the hybrid or  $\beta\text{A}$   
589 domain highlighted. **(B)** hENM extended integrin, with CG beads of  $\alpha$  and  $\beta$  chain in red  
590 and blue, respectively. **(C)** Snapshots from timestep 10 of the simulations under  $1\text{ pN}$

591 force, where the mutants (cyan, magenta and blue) are overlaid to WT (in red). **(D)**  
592 Average root mean square (RMS) displacements for WT and mutant integrins at  $F = 0-5$   
593 pN with respect to WT integrin at  $F = 0$  pN. **(E)** Average length of WT and mutant  
594 integrins at  $F = 0$  and 1pN. **(F)** Leg distance at  $F = 0-5$  pN, normalized by WT integrin at  
595  $F = 0$  pN, computed as average of the center of mass distance between the two  
596 transmembrane helices. All mean values are computed between 30-300 timesteps of  
597 simulations. Values are means  $\pm$  SEM,  $p < 0.0001$ .

598

599 **Figure 5. All-atom backmapped structures of WT and S243E under force.**

600 All-atom backmapped configurations for **(A)** wild type and **(B)** S243E integrins, after  
601 energy minimization. CG beads (in orange) and secondary structure elements (in blue  
602 and red, to distinguish between the two chains) are superimposed. AA backmapped  
603 configurations for integrins in the absence of force, embedded in multicomponent lipid  
604 bilayer, after energy minimization and equilibration: **(C)** wild type and **(D)** S243E mutant  
605 are shown in ribbon representation; lipids are shown in VDW representation. Boxplots of  
606 extension under constant force for WT and mutant integrins (computed between 100-  
607 200 ps of constant-force steered molecular dynamics simulations), normalized by the  
608 average extension of integrin without force (computed between 1-20 ns of equilibrium  
609 simulations). These values are extracted from backmapped all-atom models of WT and  
610 mutant integrins at 1 pN **(E)** and 10 pN **(F)** force. (box plots indicate median, 25th and  
611 75th percentile, min and max, \*\*\*  $p < 0.001$ , unpaired t-test).

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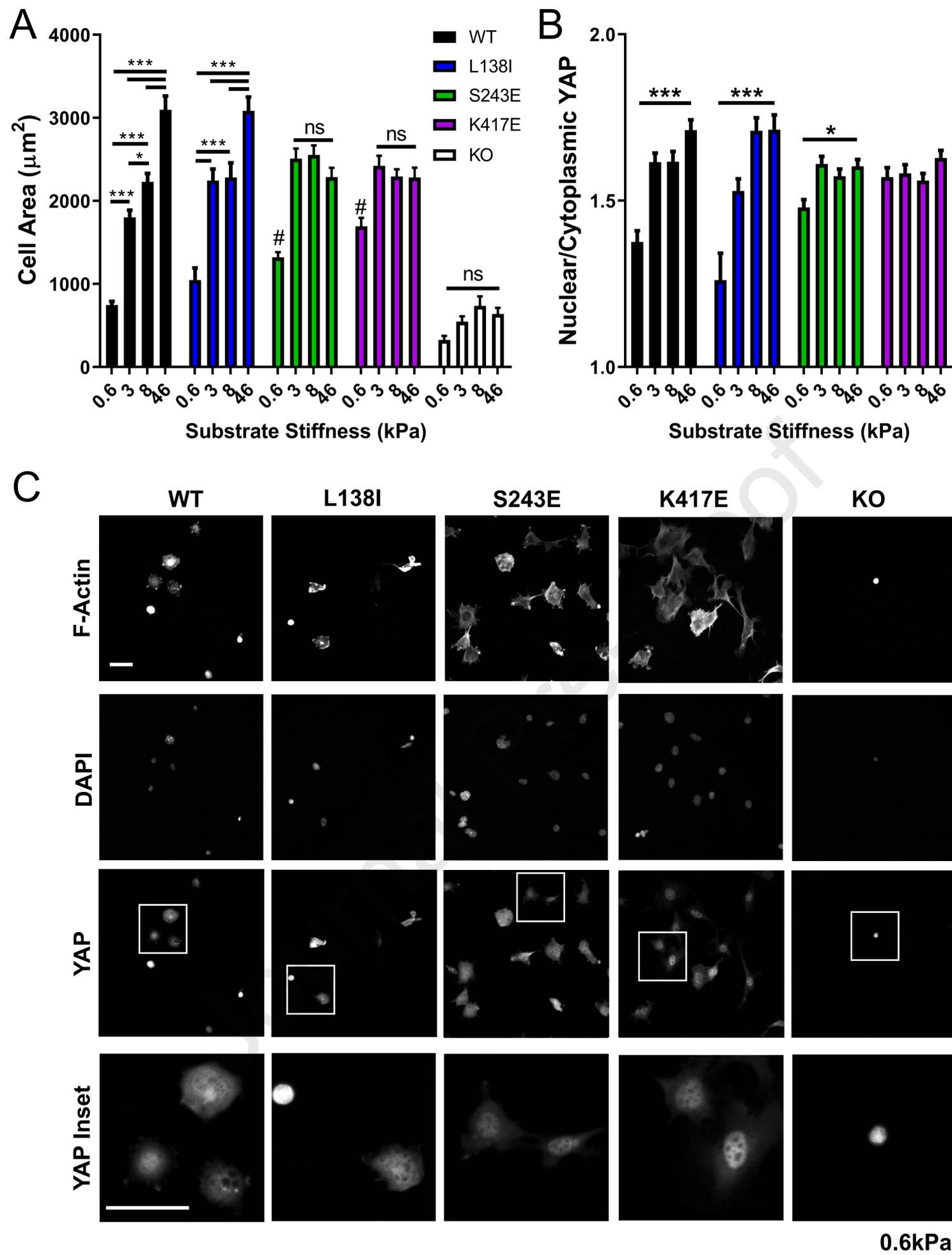
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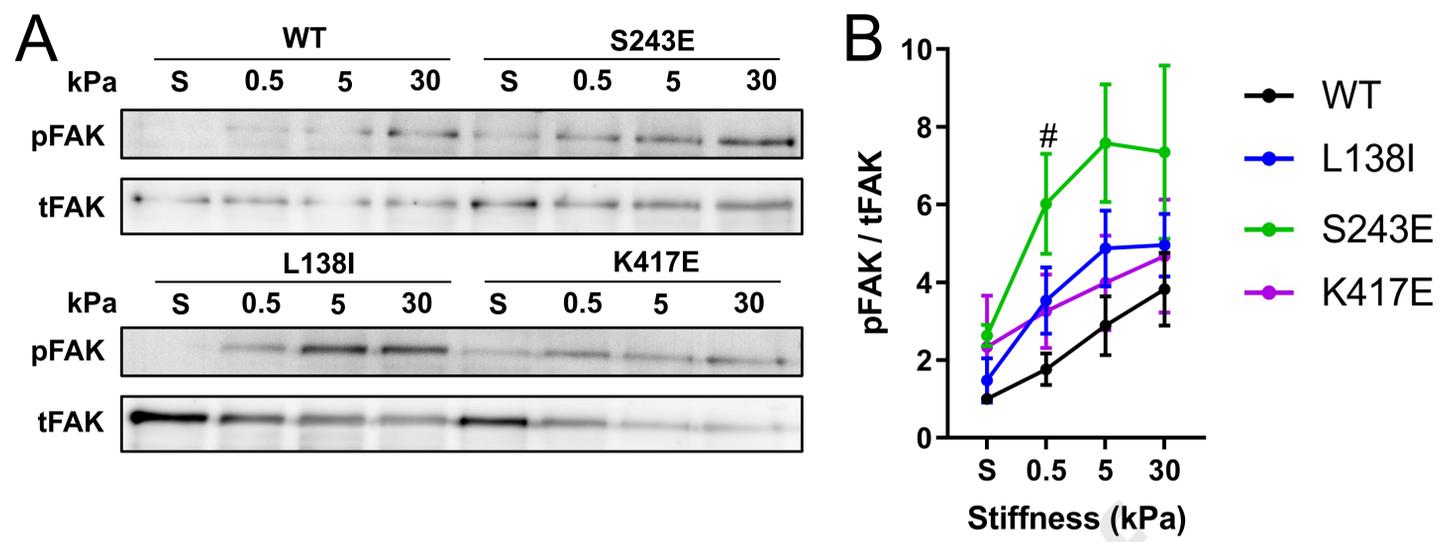
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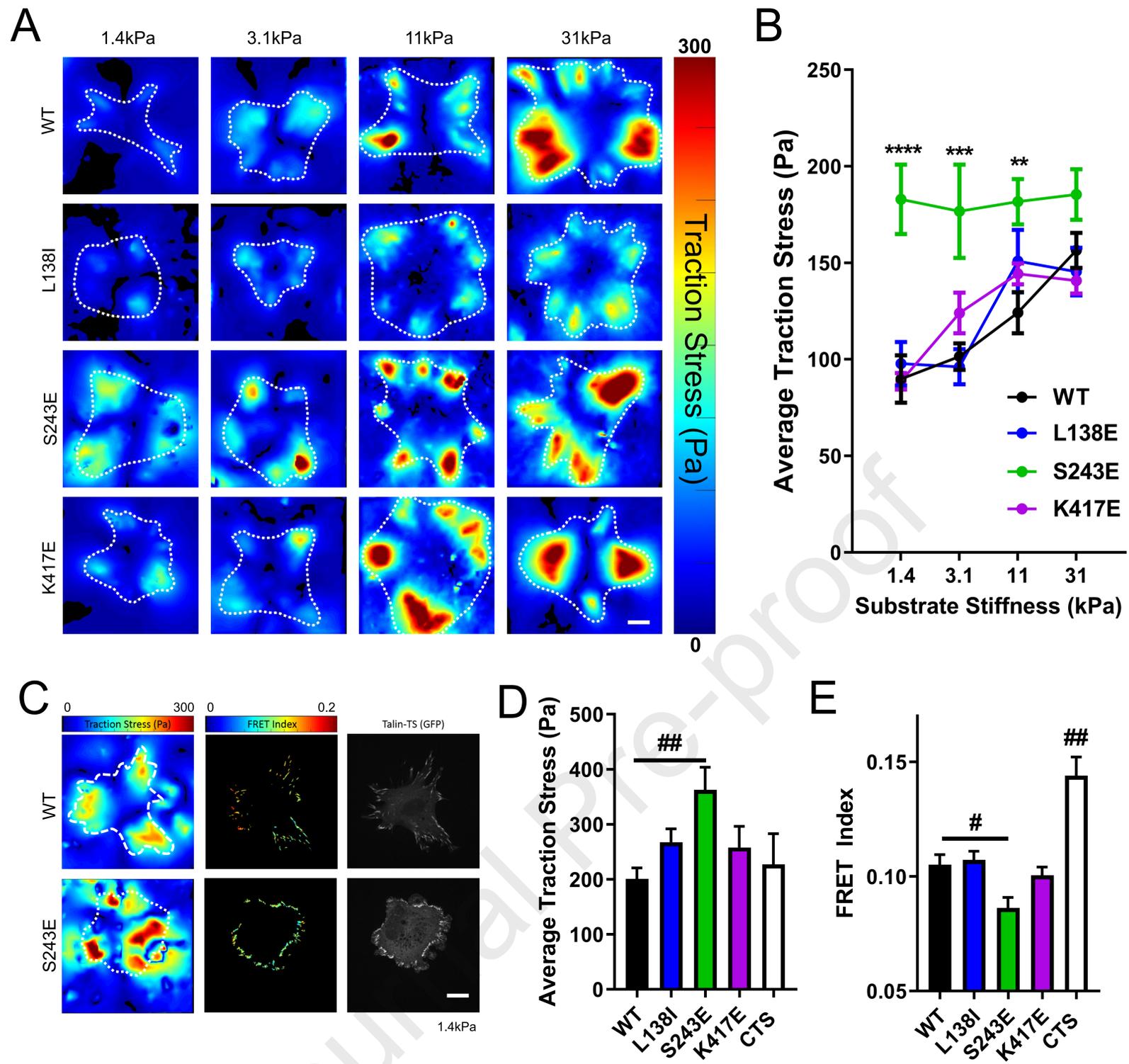
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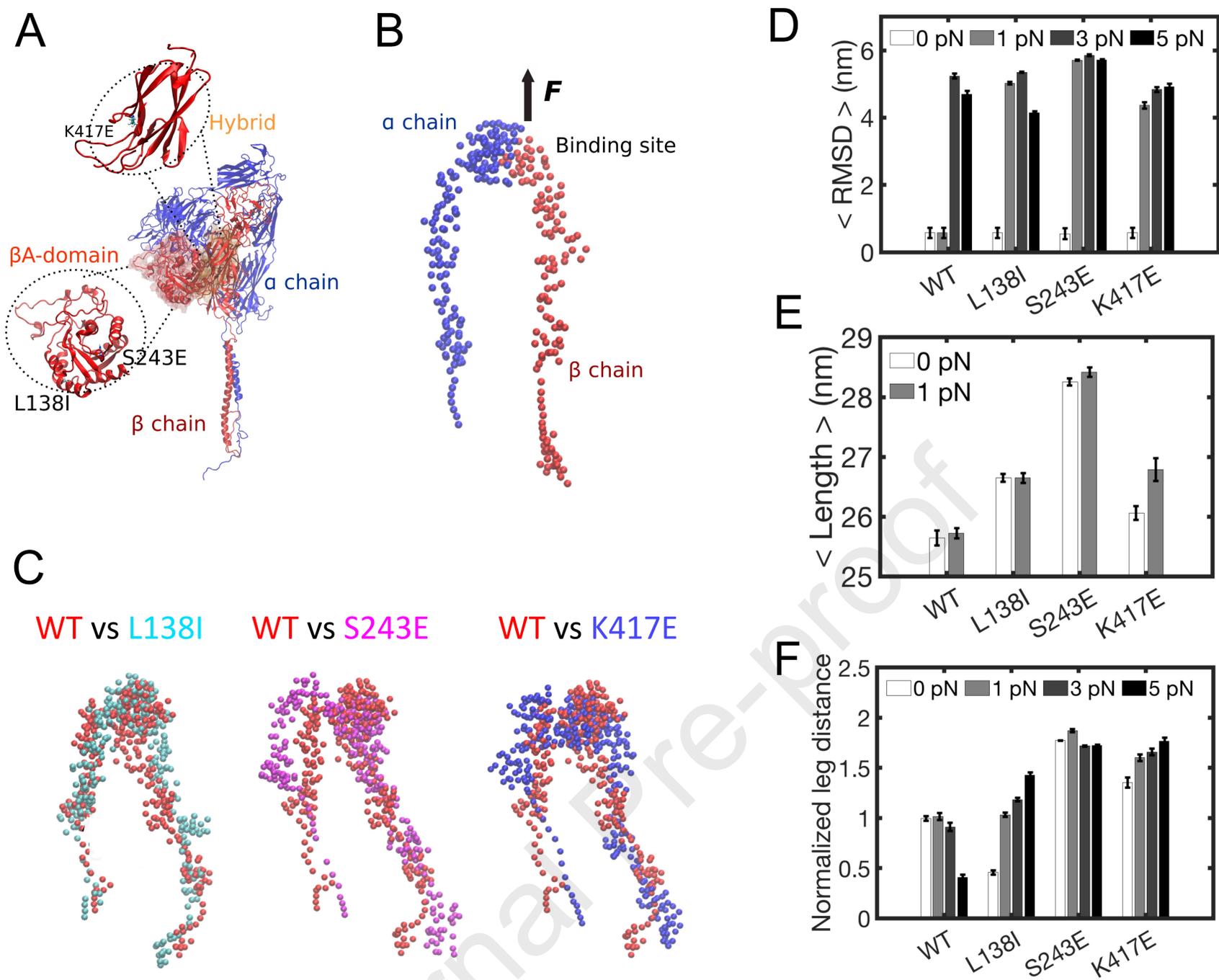
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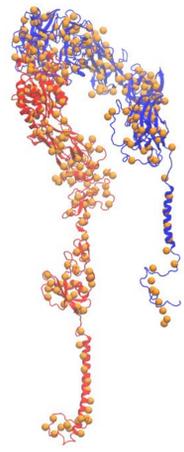




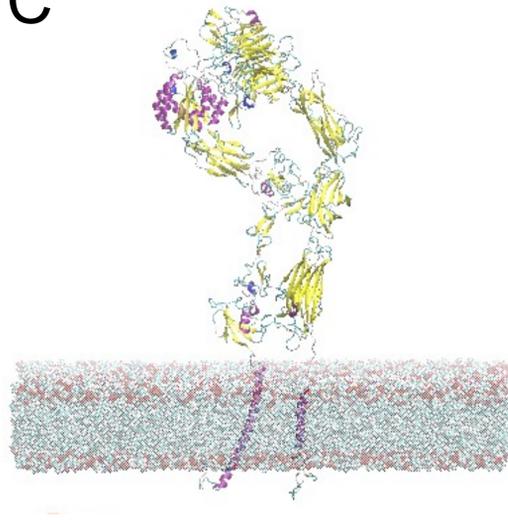




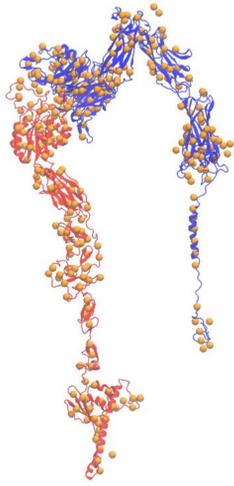
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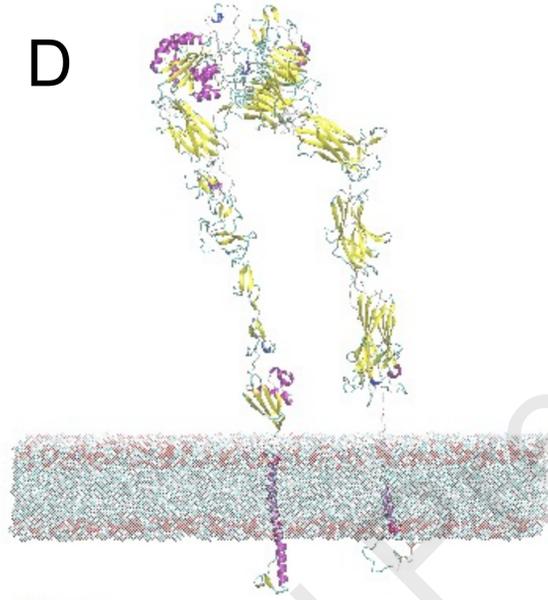
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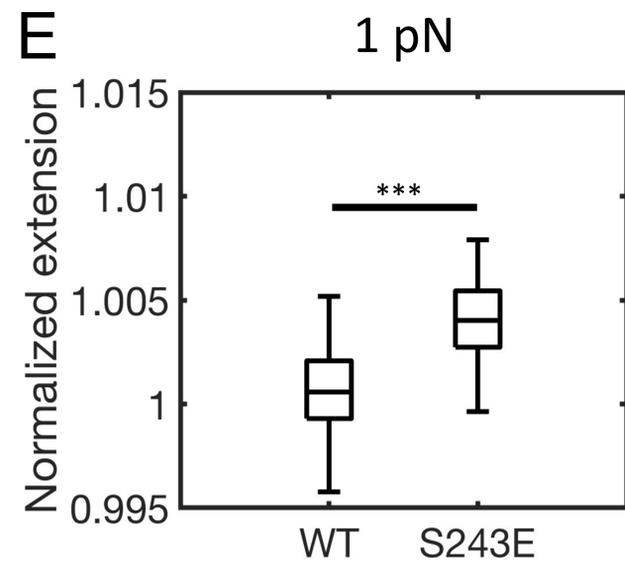
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